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UTAH GEOLOGICAL AND MINERAL SURVEY

NO. 139

GEOHERMAL INVESTIGATIONS
AT
CRYSTAL HOT SPRINGS
SALT LAKE COUNTY, UTAH

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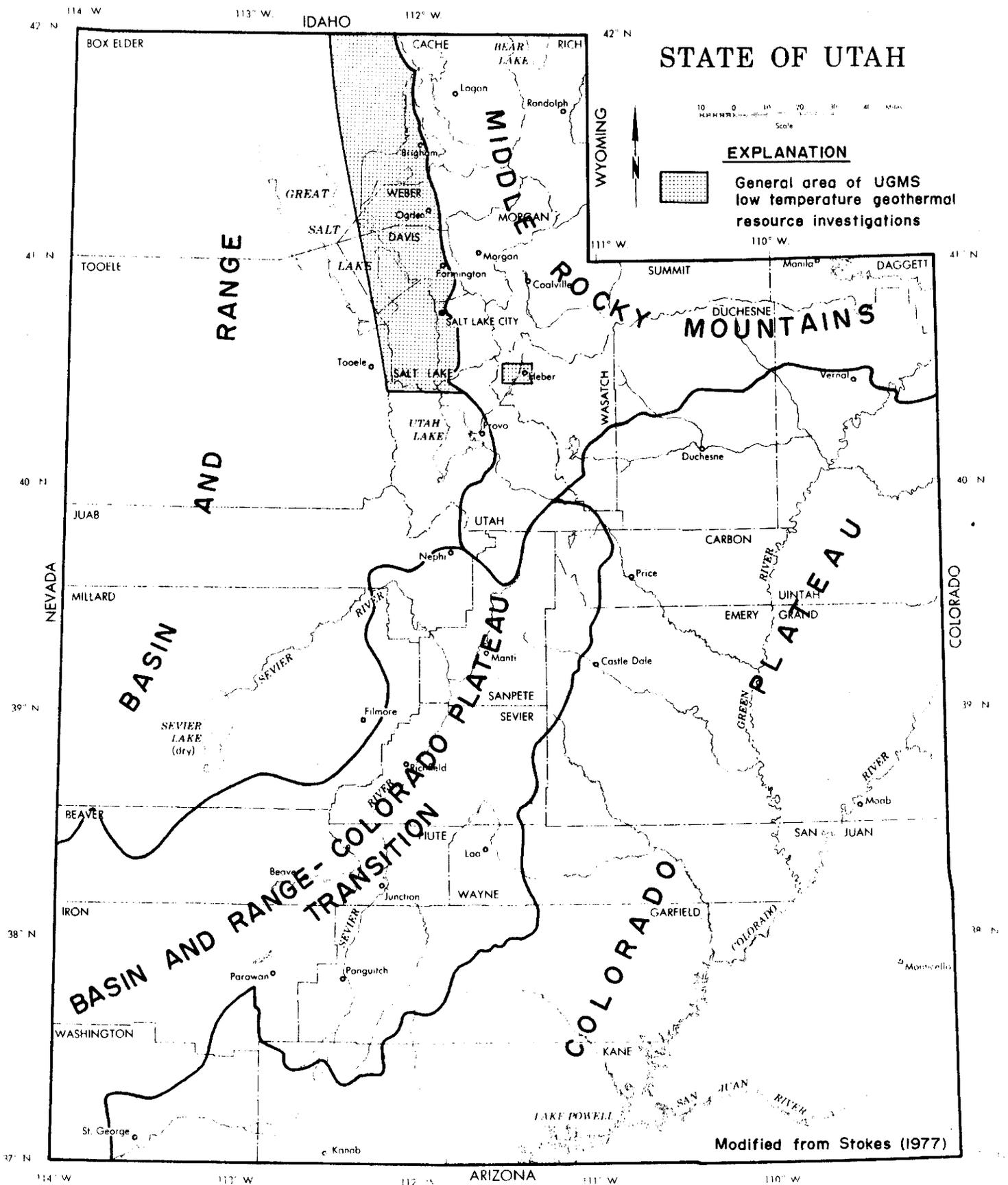
ABSTRACT

The Crystal Hot Springs geothermal system is located in southern Salt Lake County, Utah 22.5 km (14 miles) south of Salt Lake City near the town of Draper. The system is immediately west of the Wasatch Mountains at the easternmost edge of the Basin and Range physiographic province within an active seismic zone referred to as the Intermountain Seismic Belt. The springs are located north of an east-west trending horst known as the Traverse Range. The range is intermediate in elevation between the Wasatch Range to the east and the valley grabens to the north and south. A series of north-east striking normal faults with a combined displacement of at least 900 m (3,000 ft.) separate the horst from the Jordan Valley graben to the north. The spring system is located between two closely spaced range-front faults where the faults are intersected by a north-northeast striking fault. The fractured Paleozoic quartzite bedrock 25 m (80 ft.) beneath the surface leaks thermal water into the overlying unconsolidated material and the springs issue along zones of weaknesses in the relatively impermeable confining zone that parallel the bedrock faults. Meteoric water from the Wasatch Range is warmed in the normal geothermal gradient of the province (approximately 32° C/km) as the water circulates to a minimum depth of approximately 2.5 km (1.55 miles) via an undetermined path through aquifers and faults. Data collected at the Crystal Hot Springs system under the DOE state coupled program is presented for use by individuals interested in the system.

INTRODUCTION

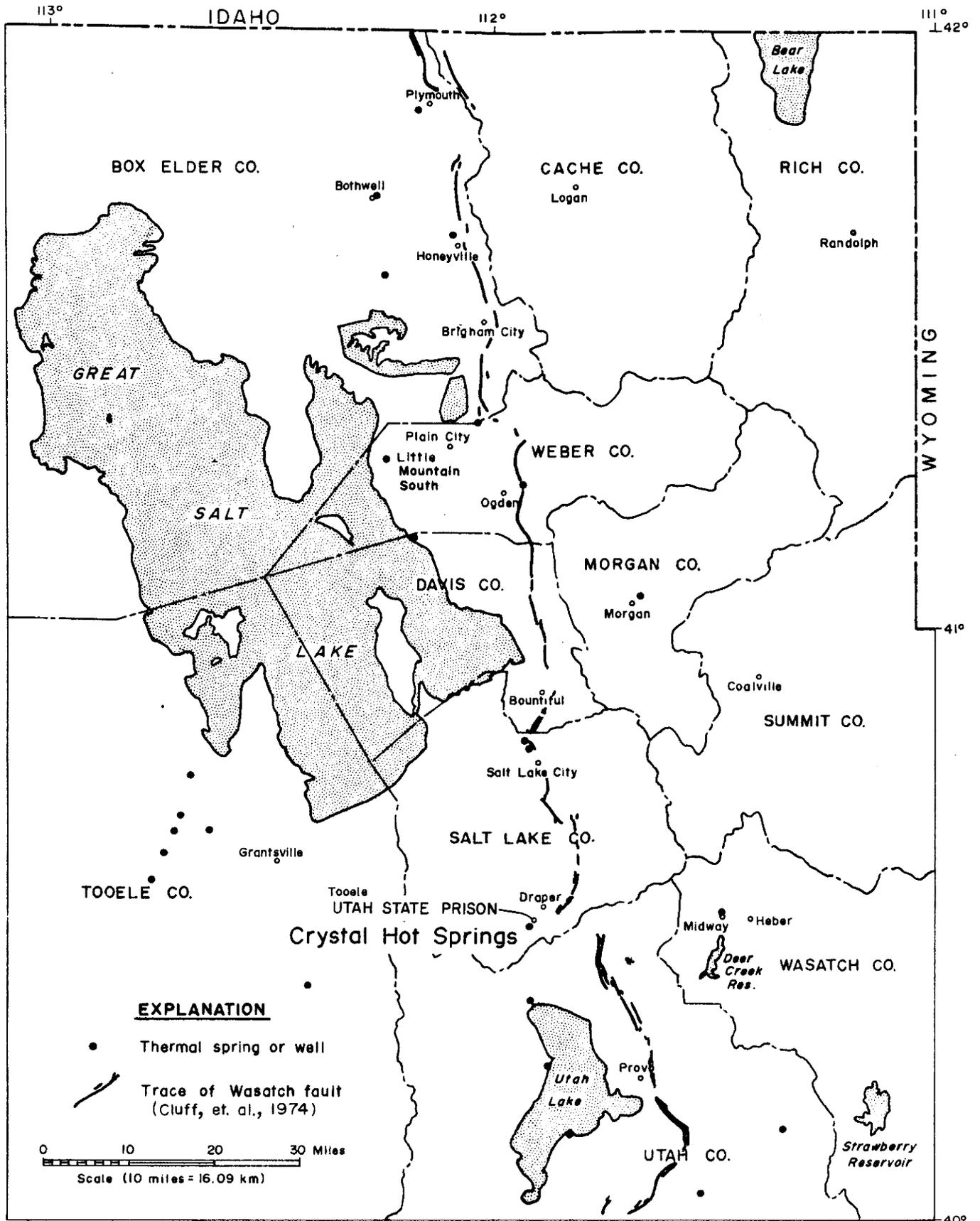
Under contract with the U. S. Department of Energy/Division of Geothermal Energy (DOE/DGE), the Utah Geological and Mineral Survey (UGMS) has been conducting research to advance the utilization of low temperature geothermal heat in the state of Utah. Activities related to the contract (originally EG-77-S-07-1679 but later changed to DE-AS07-77ET28393) began on July 1, 1977 and will continue into 1980.

To date, UGMS has concentrated its investigations along the Wasatch Front from Utah Valley on the south to the Utah-Idaho state line on the north (figures 1 and 2). The reasons for the



Index map showing major physiographic provinces of Utah

Figure 1



Index map of northern Utah with the locations of Crystal Hot Springs and other major thermal springs of the Wasatch Front.

Figure 2

concentration of effort in this area of the state are as follows: 1) the concentration of apparent geothermal resources in this area and 2) the three major population centers of the state: (north to south) Ogden, Salt Lake City, and Provo lie within the region. The co-location of low temperature geothermal resources and potential users increases the possibility of timely resource development. Therefore, resource definition in populated areas should encourage the development of low temperature resources for direct heat applications by providing a data base from which potential users can make informed decisions. At the same time, investigations of the Basin and Range Province geothermal systems of the Wasatch Front will provide data for models that will be applicable to other Basin and Range geothermal systems.

In addition to the reasons cited above, the investigation of the Crystal Hot Springs geothermal system in southern Salt Lake County (figure 2) was initiated because of the apparent high quality of the resource. The maximum measured temperature of the system (86°C) and the geothermal fluids containing approximately 1500 mg/l TDS, combine to make this geothermal system attractive from the standpoint of use and disposal. Should the quality resource prove to be more wide spread at depths of 305 m (1,000 ft.) or less than presently indicated by the existing surface expression of the hot spring system, a wide variety of uses might be made of the geothermal fluids.

The following report of investigation represents the present state of knowledge of the Crystal Hot Springs geothermal system and the surrounding area. Additional investigations are planned for this resource area under the DOE/DGE state coupled program and a P.O.N. (project opportunity notice) award to the State of Utah by DOE/DGE for the State Prison facilities at Point of the Mountain. Reports on future investigations will be made available as progress continues.

REGIONAL GEOLOGIC AND STRUCTURAL SETTING

The Salt Lake area lies at the intersection of three major tectonic elements: 1) the Uinta Arch (figures 3 and 4), 2) the Thrust Belt (figures 3 and 4), and 3) the Intermountain Seismic Zone (figure 6).

Uinta Arch

The Uinta Arch, a broad anticlinal structure, is a westward continuation of the anticlinal structure of the Uinta Mountains. The axis of the fold in the Wasatch Mountains strikes N60°E, dips 30°E, and is exposed along the Wasatch Front just north of the mouth of Little Cottonwood Canyon. North of the Uinta Arch axis is a broad syncline referred to as the Parleys Canyon synclinorium (figure 4), a multiple fold structure containing two smaller synclines and a tight anticline. The axis of the

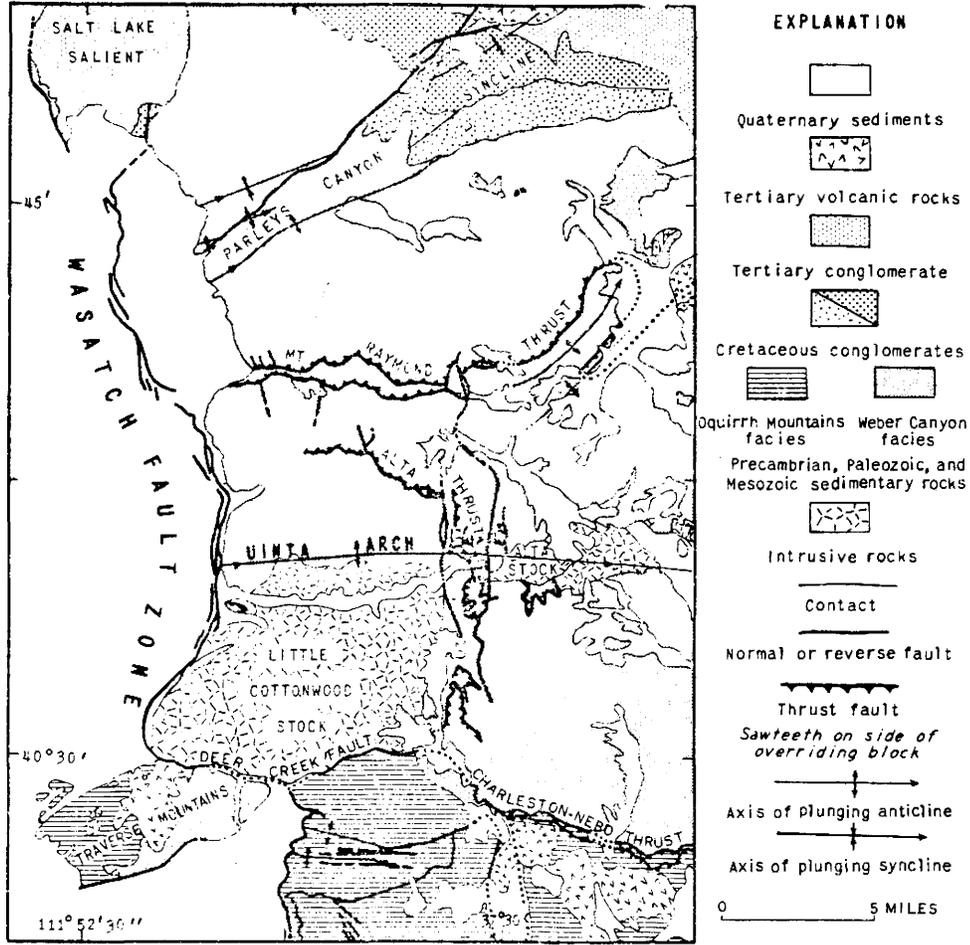


Figure 4. Internal structure of the Wasatch Range east of Salt Lake County, Utah (from Crittenden, 1964).

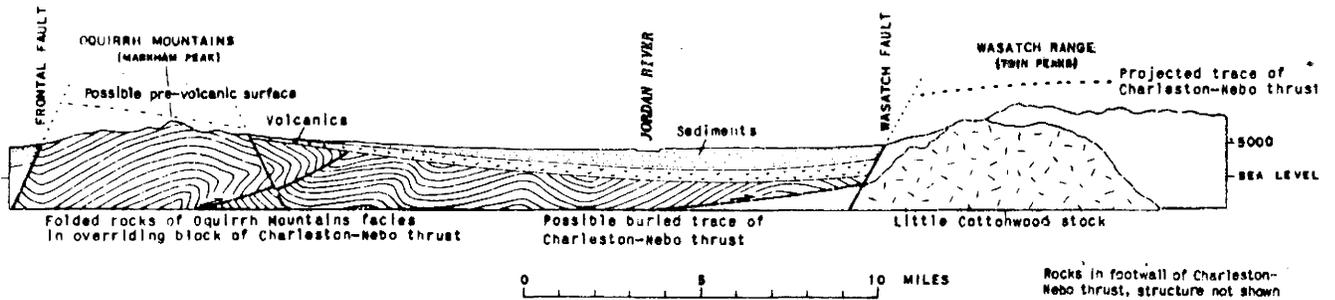


Figure 5. Generalized cross section from Markham Peak in Oquirrh Mountains through Twin Peaks in Wasatch Range. (Modified from Crittenden, 1964).

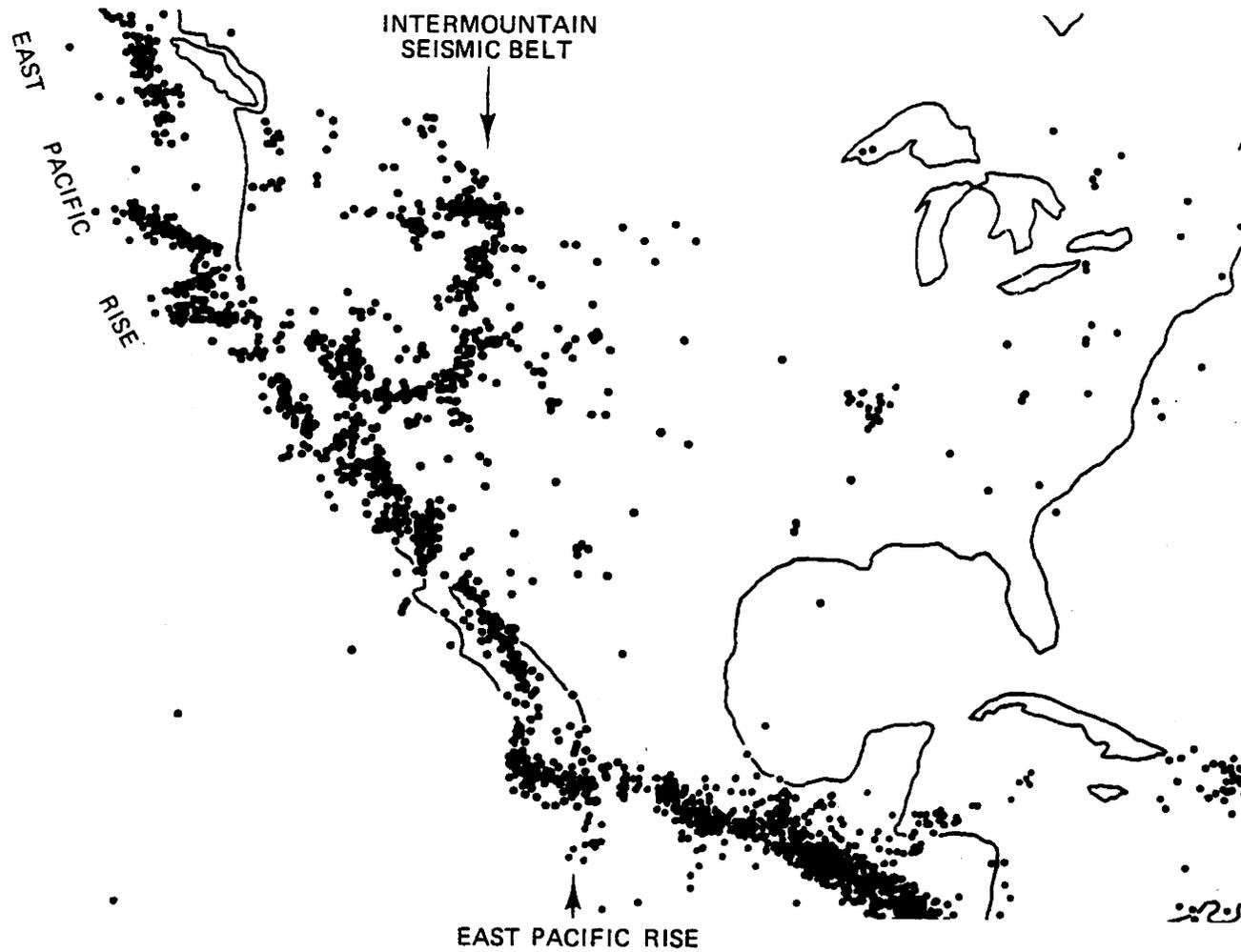


Figure 6. Earthquake epicenters in United States and adjacent regions during 1961-67. Note northward-trending Intermountain Seismic Belt extending through central Utah (Cook, 1971).

Parleys Canyon synclorium is sub parallel to the axis of the Uinta Arch. Precambrian to Jurassic rocks are present in the folds. Uplift and deformation of the Parleys Canyon syncline occurred in three pulses: 85-90, 75, and 60-70 million years ago (Crittenden, 1964).

Thrust Belt

East to west thrusting occurred during the Laramide orogeny and is represented in the Salt Lake area by three recognized thrust sheets (figure 4). The Alta and Mount Raymond thrusts are present to the east and north of the Little Cottonwood stock and are approximately 125 and 85-90 million years old respectively (Crittenden, 1964). The Charleston-Nebo thrust fault (figures 3 and 4) has a total displacement of 64 km (40 miles) or more, and is the youngest thrust identified in the Salt Lake area at 75-80 million years old (Crittenden, 1964). Evidence for the Charleston-Nebo thrust is present in the Wasatch Mountains (figure 4), but the inferred trace of the fault has been extended westward through the Wasatch, between the East Traverse Range and the Little Cottonwood stock. The fault also extends north and west of the area between the Oquirrh Mountains and Antelope Island to be linked with the Willard thrust east of Ogden (figure 3). This interpretation of thrusting in the Salt Lake area places both the Traverse Ranges and the Oquirrh Mountains on the thrust plate, and explains the differences in geology between the Wasatch and Oquirrh Ranges. The thrust plane of the Charleston-Nebo thrust dips westward (figure 5) and may be as deep as 3.2-8.0 km (2 to 5 miles) beneath the Oquirrh Mountains. Northwest striking folds present in the southern Oquirrh Mountains and the West Traverse Range may have been formed during thrusting, as wrinkles on the upper plate. (Crittenden, 1964).

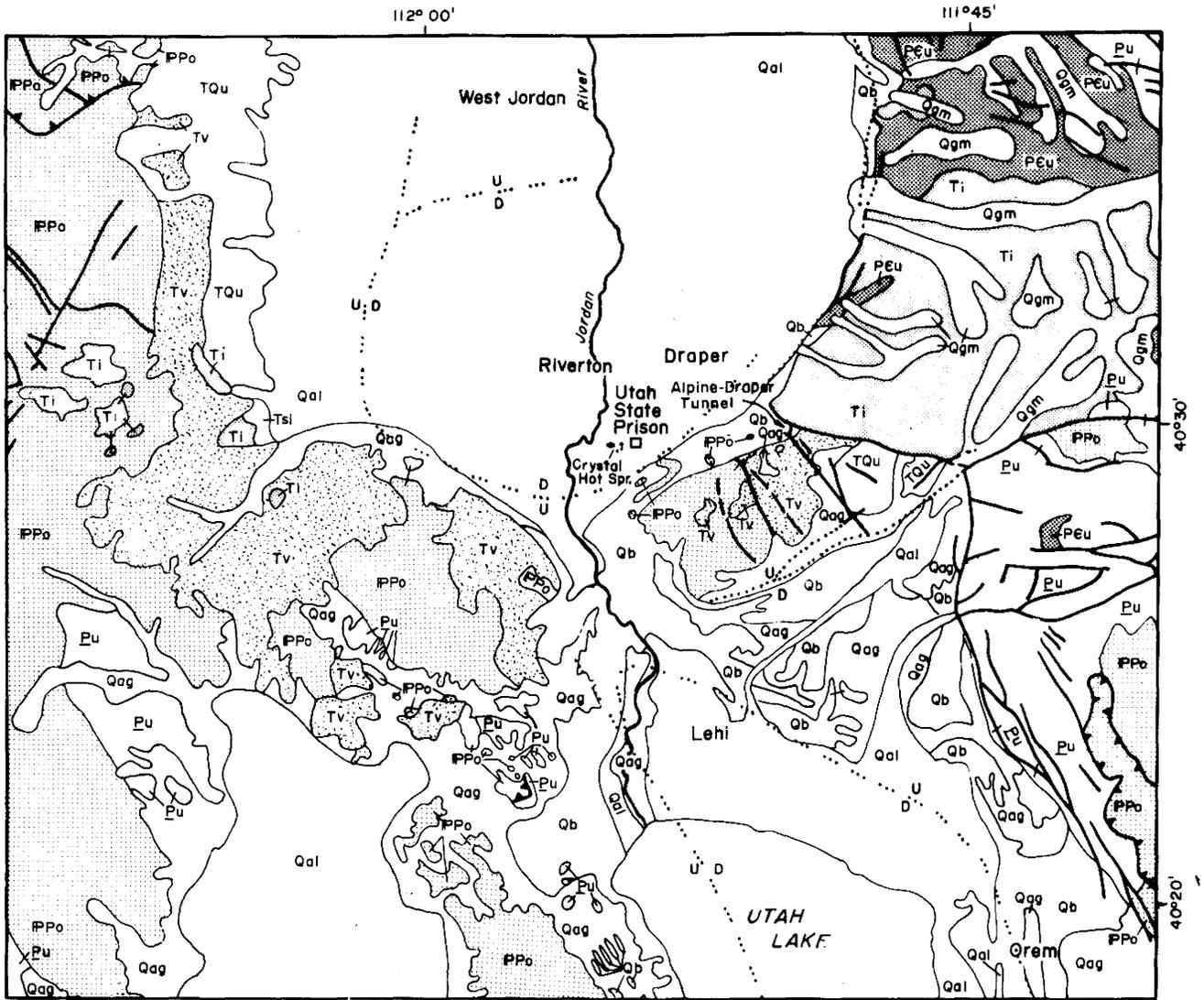
Intermountain Seismic Belt

The Intermountain Seismic Belt is a 100 km wide zone of relatively high seismicity, extending from northern Arizona to northwestern Montana (figure 6) and locally coincident with the Wasatch Front. This zone parallels the eastern margin of the Basin and Range physiographic province; seismic studies by Smith and Sbar (1970), and Shur and Barazongi (1970) suggest the zone is an active rift system with the tensional axis orientated in an east west direction. The tensional forces are those that, over the past 20 to 25 million years, have produced the fault block mountains of the Basin and Range province.

THE TRAVERSE MOUNTAINS

Geology

In greatly simplified terms, the Traverse Ranges can be described as folded and fractured Paleozoic limestones and quartzites, mantled in places by Tertiary volcanics, and Quaternary sediments of



EXPLANATION

Qal	Quaternary alluvium	Tsi	Tertiary - Salt Lake group	Fault: Well exposed
Qag	Quaternary colluvium and alluvium	Ti	Tertiary intrusives	Inferred
Qb	Quaternary - Bonneville related sediments	Tv	Tertiary volcanics	Covered by alluvium
Qgm	Quaternary glaciated ground and moraines - undifferentiated	PPo	Permian & Pennsylvanian Oquirrh formation	Thrust fault - barbs on upper plate of thrust sheet.
Tqu	Tertiary - Quaternary deposits - undifferentiated	Pu	Paleozoic sedimentary units, undifferentiated	Fault - inferred from geophysical evidence
PCu	Precambrian sedimentary units - undifferentiated			

0 5 Miles
Scale
(1 Mile = 1.61 Km)

Modified from Geologic Map of Utah, NW 1/4, 1963, compiled by W.L. Stokes

Geology of the Traverse Mountain Region, Utah

Figure 7

varying origins. The following is a brief description of the rocks of the Traverse Ranges.

Paleozoic System

The Paleozoic rocks of the Traverse Ranges are predominately Pennsylvanian rocks of the Oquirrh Formation (Marsell, 1932) (figure 7). Manning Canyon shale of Mississippian-Pennsylvanian age, and Mississippian Great Blue limestone are present on the south flank of the West Traverse range, but are only exposed in relatively small areas (Pitcher, 1957). Bullock (1958) assigned a total thickness of 1,524 m (5,000 feet) to the Oquirrh Formation in the Lehi quadrangle, and Pitcher (1957) reported the Oquirrh Formation in the Jordan Narrows quadrangle to be approximately 1,128 m (3,700 feet) thick. Pitcher's (1957) stratigraphic column has been reproduced here in figure 8, where the lithologies of the Marrowan, Attokean, and Desmoines series of the Oquirrh Formation are described. Marsell (1932) indicates that the most abundant rock type in the ranges is quartzite, and less often limestone and sandstone can be found. Pitcher (1957) mapped large areas of the Desmoines series in the Jordan Narrows quadrangle.

The Paleozoic rocks are present through the Traverse ranges, even where Tertiary volcanics and Quaternary deposits are present at the surface (figure 7).

Tertiary System

Sedimentary Rock: Slentz (1955) noted and described four units of the Salt Lake group in the vicinity of the Jordan Narrows. In order of decreasing age, the units are: 1) the Jordan Narrow unit consisting of marlstones, 2) the Camp Williams unit consisting of poorly consolidated mudstones and siltstones, 3) the Travertine unit that, in places, resembles tufa, and 4) the Harkers fanglomerate displaying torrential bedding and cut-and-fill structures.

The Travertine unit: “. . . varies from dense, massive flinty travertine to coarse, crustiform, or even cavernous, limestone, often resembling tufa” (Marsell, 1932) contains lenses of manganese ore, and was deposited by hot spring activity. The age of the unit has been established as late Pliocene by identification of a jaw bone and teeth found in the travertine by Marsell (Slentz, 1955). Slentz (1955) shows three locations where the Travertine unit is present, the northern and westernmost of the three exposures are on strike with the westward extension of the Steep Mountain fault line scarp (figure 21a).

Volcanics: Tertiary volcanics in the Traverse ranges (figure 7) are primarily andesitic lava flows that vary in composition. Marsell (1932) described the volcanic rocks in some detail and found that in the East Traverse mountains the lavas were principally andesite porphyries and augite-andesite porphyries. In the West Traverse mountains the composition varied from sub-basic augite prophyry to

augite latities; four sets of flows were identified.

The lavas were extruded during the late Oligocene or early Miocene through vents at South Mountain and Step Mountain in the West Traverse range. No such vents were found in the East Traverse range. The first lavas were extruded on to a deeply eroded surface, and weathered surfaces on some flows indicate that eruptive events were separated by time.

The scattered distribution of lava flow remnants throughout the Traverse ranges (figure 7), is an indication that the flows were at one time more extensive than at the present and may have covered adjacent portions of the Oquirrh and Wasatch mountains (Marsell, 1932). At the present time the volcanics flank the eastern edge of the Oquirrh Mountains south of Copperton; extending south and southeast to cover a large area of the western West Traverse range. A second major area of volcanics covers the northeast corner of the western range, while small patches of volcanics dot the southern flank of the range. About one third of the bedrock surface in the Eastern Traverse range is covered by volcanics, though exposures are limited to the eastern portion of the range (figure 7).

Intrusives: Two areas containing large igneous intrusions are present in the vicinity of the Traverse ranges (figure 7): the Little Cottonwood-Alta stock, and the Bingham Canyon area. The granitic intrusions of the Little Cottonwood area were emplaced between 41 - 24 million years ago with the Little Cottonwood stock being emplaced 24 -31 million years ago (Crittenden, et. al, 1973). The quartz monzonite intrusions in the Bingham area were emplaced during the late Eocene or early Oligocene (Bray, et. al., 1975).

In the West Traverse Mountains near their junction with the Oquirrh Mountains are four volcanic plugs or necks and one small stock (Marsell, 1932). Marsell describes the stock at Shaggy Peak as a “. . . rounded hill of rhyolite porphyry, surrounded on all sides of flows of andesite breccia and latite”. According to Marsell, Step Mountain is a volcanic neck, and South Mountain is a group of three volcanic necks. The rock in all four of the necks is mica-andesite prophyry.

Quaternary System

Deposits of Quaternary age that have been recognized in the Traverse Ranges include: 1) Pre-Lake Bonneville fans, 2) the Lake Bonneville group consisting of the Alpine and Bonneville and Provo formations, and 3) post-Provo deposits. The prominent spit at the western end of the East Traverse range is a portion of the Bonneville Formation, as are the discontinuous beach deposits along the north flank of the range.

TERTIARY QUATERNARY		Formation	Thickness	Description	Section
				Gravel, sand and silt.	
		Salt Lake group	600 +	Marlstone, siltstone, limestone, tuff and conglomerate.	
PENNSYLVANIAN		Oquirrh	1,000 +	<u>Desmoines series</u> Light brown to tan quartzite with some medium gray orthoquartzite interbedded with a few light to medium gray beds of limestone.	
			1,913 ±	<u>Atokan series</u> Medium to dark gray, sandy limestone that weathers light gray, interbedded with light brown to tan cross-bedded orthoquartzite.	
		Formation	854	<u>Morrowan series</u> Limestone; medium to dark gray, medium to thick bedded, fetid in part, sandy, with some cherty beds.	
		Manning Canyon shale	1,200 ±	Shale; light brown to black with some quartzite and limestone beds. Springeran probably begins at the bottom of the prominent bed of scintillating quartzite.	
MISSISSIPPIAN		Great Blue limestone	800 +	Limestone; medium gray, weathering light gray, medium to thick bedded and platy in places, sandy.	

Figure 8. Stratigraphy of the Jordan Narrows quadrangle (Modified from Pitcher, 1957).

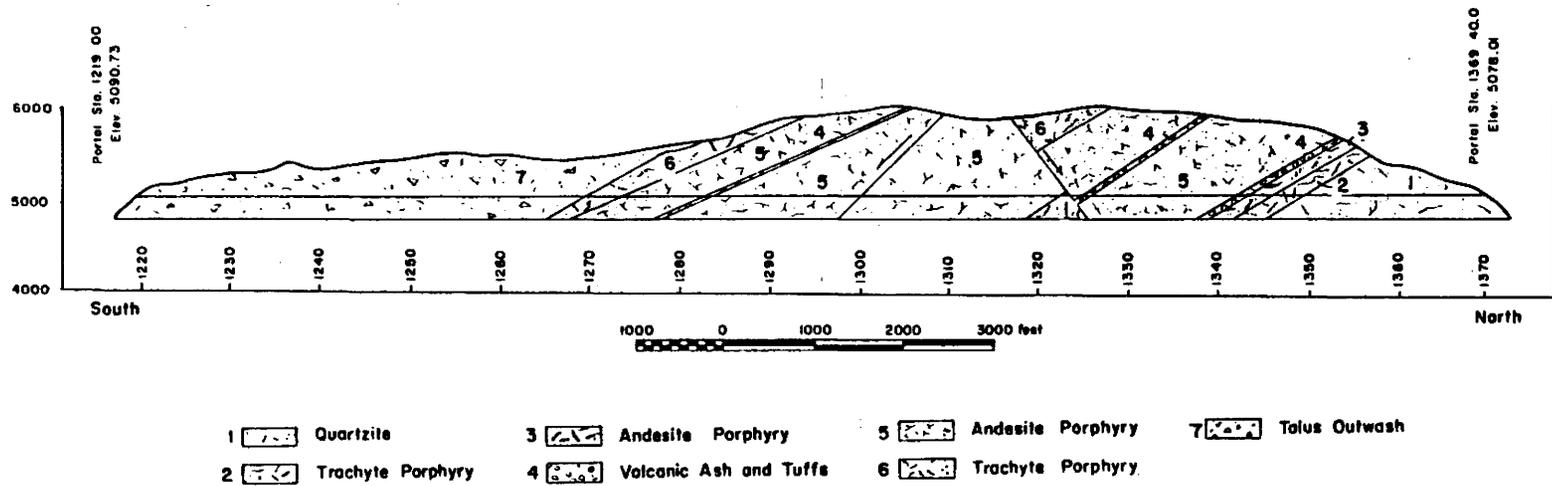


Figure 9. Structural section along Alpine-Draper Tunnel after J. N. Murdock September 1941. Cross-section from (Bullock, 1958).

Structures Bounding the Traverse Mountains

The Traverse Ranges trend east-west in a region where the prevailing structural trends are north-south (figure 7), and as a result, the structural detail is complex. The northern edge of the Traverse Ranges is bounded by a series of normal faults that separate the ranges from the Jordan Valley graben (figure 7) to the north (Cook and Berg, 1961). Striking almost east-west and dipping southward, the main branch of the Wasatch fault separates the eastern end of the East Traverse mountains from the Little Cottonwood stock (figure 7). Although no fault has been found on the southern flank of the Western Traverse range, a series of normal faults similar to those on the north flank separate the East Traverse range from the Utah Valley graben to the south (Cook and Berg, 1961). Marsell (1932) reports that the folds of the Oquirrh Mountains could be traced into the West Traverse range, and the ranges were not separated by Basin and Range faulting.

Internal Structures of the Traverse Ranges

Marsell (1932) describes the Western Traverse Range as “. . . a homoclinal succession with a general east-west strike, and a north dip which averages 35° . As a junction of the range with the Oquirrh Mountains is approached, the strike swings more to the northwest, in conformity with the trend of the east limb of the Tickville Gulch anticline in the latter range”.

Marsell (1932) viewed the East Traverse mountains as a “steeply pitching anticlinal nose, which, in the vicinity of the Jordan Narrows, appears to merge with the homocline of the West Traverse mountains”. As evidence for the anticlinal nose structure, Marsell sites the “general” dip of the rocks on the north flank to the north, the south flank to the south, and the rocks near the Jordan Narrows to the west; measured strikes and dips are not given. Bullock (1958) presents a cross-section, shown here in figure 9, through the East Traverse mountains that was prepared along the Alpine-Draper Tunnel by J. N. Murdock (1941). The location of the cross-section near the eastern end of the range is indicated in figure 7. The apparent dips of the rocks, as observed in the cross-section, are all southward at approximately 23° . Neither Pitcher (1957) nor Bullock make any suggestions concerning the overall structure of the ranges, however there is considerable doubt that Marsell's interpretation of the internal structure of the East Traverse range is correct.

One of the difficulties encountered when working in the Traverse Ranges is the highly fractured nature of the rocks. The intense fracturing along with the well developed soil cover are undoubtedly the reason for the lack of good geologic and structural information. Marsell (1932) was, however,

able to identify a series of north-northwest trending faults in the East Traverse Ranges (figure 7) that were determined to be older than the Tertiary volcanics that once covered the range. Marsell suggests these faults were formed at the time of the anticlinal folding, and notes how the faults have the same trends as the large scale folding in the Oquirrh Mountains.

DESCRIPTION OF CRYSTAL HOT SPRINGS

The surface expression of the geothermal resource at the Point of the Mountain is restricted to a group of springs known as Crystal Hot Springs, which are found within an area of approximately 70 acres bounded by the Utah State Prison farm on the north, the Utah State Prison minimum security buildings on the east, the Bluffdale Road on the south, and by a number of small farms on the west. No surface expressions of the Crystal Hot Spring system have been found outside of this area.

There are large number of spring orifices associated with the Crystal Hot Spring system (figure 10). Some of these orifices are beneath the surfaces of the small ponds located near the eastern edge of the system, and a few are present at the bottom of the large western lake. The remainder of the orifices are found in the bottoms of relatively small circular depressions near the southern boundary of the area and north of the large western lake.

Although water at the surface of the eastern ponds feels only warm to the touch, temperatures as great as 84°C have been measured at spring orifices within the lake muds. The water from the springs drain northward through a series of channels connecting individual ponds. The total flow from the eastern lakes is diverted westward through a drainage ditch to the large western lake, (figure 10).

The western lake is at least 15 meters deep, and is divided into two basins by a ridge that almost reaches the surface of the lake. The owner of the spring has indicated that at one time a heavy weight was lowered into one of the orifices and no bottom was encountered; he estimated the total depth of the lake to be approximately 90 meters (300 feet). Divers who have been in the lake on a number of occasions, however, found the maximum depth of the lake to be approximately 15 meters (50 ft.). Bottom mud temperatures as great as 82°C have been measured in this lake.

Taylor and Leggette (1949) report the results of a pump test in which the western basin of the large western lake was pumped at a rate of 8.6 feet³/sec. for 26 hours. Important results of this test are as follows:

- 1) The pumping exposed several small orifices of the eastern edge of the lake that remained several inches above the fluctuating level of the lake.
- 2) After removing a total 9.86 acre-feet of water, the lake refilled at a rate that decreased from

1.30 feet³/sec. to 1.12 feet³/sec. as the lake returned to pre-test levels.

- 3) The springs in the western portion of the lake produce water at a rate of approximately 1.13 feet³/sec.
- 4) Water levels in auger holes to the north and south of the lake did not fluctuate as the lake level decreased.
- 5) Drawdown in the western lake did not induce drawdown in the eastern ponds.

Further details of this test are given in the reference cited above and the same account is reproduced in Goode (1978).

Most of the combined spring outflow drains out the western end of the lake through a pipe and into a drainage ditch. However, a tropical fish hatchery and a beaver farm divert some of the water for heating purposes before discharging this water into the same ditch. The water eventually drains into the Jordan River.

In addition to the hot spring orifices that are associated with the western lakes and eastern ponds, there are two areas where springs and seeps occupy the bottoms of small circular depressions. In the bottoms of some of the depressions only damp soil is present, while in others standing water less than 1 meter deep is found. In both areas, there is little or no flow away from the springs. Ten to twenty of these orifices are found in an east-west trending zone that begins south of the eastern ponds and ends south of the western lake. Just north of the western lake are about 5 depressions measuring from one to five meters across and containing up to several meters of standing water.

Water level information in the vicinity of Crystal Hot Springs is presented in figure 11. Contours in this figure represent the water surface level of ponds without outlets in the spring system, relative to the pond which is located to the northwest of the large western lake. The water surface in the area conforms to the topography of the spring site. The approximate elevations to which water rises in water wells within the area is also indicated. Depth-to-water in each hole was measured when access to the hole was obtained; measurements span a period of one year. The regional flow of groundwater is to the north and west away from the springs.

Other Occurrences of Warm Water

Although Crystal Hot Springs is the only source of water above 30°C in the southern Jordan Valley, additional occurrences of warm water have been reported. In the Jordan Narrows, the Camp Williams warm spring (C-4-1) 23 bcb issues in the vicinity of Tertiary tufa deposits at a temperature

of approximately 23°C (figure 21). Further south in the Jordan Narrows, Milligan, et. al. (1966) reported the presence of 27°C water 6 feet below the surface where the Provo Reservoir Canal crosses the Jordan River (C-4-1) caa (figure 21). Warm water (21-25.5°C) at depths of less than 180 m has also been reported in Draper area, (D-3-1) 29, water wells.

Ten miles due south of Crystal Hot Springs in Utah Valley are two hot springs. Saratoga Hot Spring, (C-5-1) 25 cd, on the northwest shore of Utah Lake flows to the surface at 38 to 44°C. One mile east-northeast of Saratoga, in Utah Lake, is Crater Hot Spring with reported temperatures ranging from 42-44°C.

SHALLOW GROUND TEMPERATURE SURVEY

Techniques

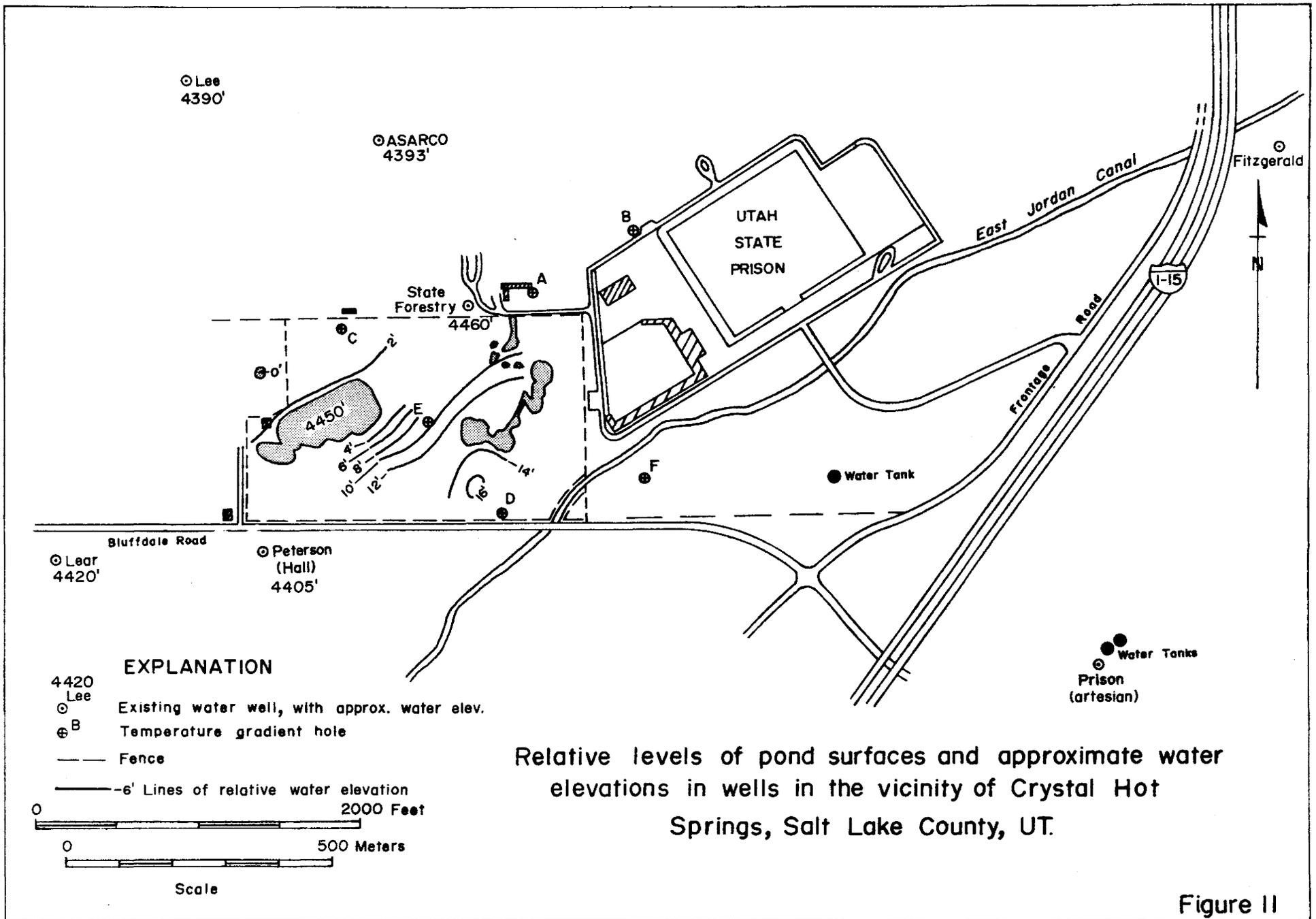
A detailed shallow ground temperature survey was conducted in the immediate vicinity of the Crystal Hot Spring system to determine if the temperature of the ground at a depth of approximately one meter could yield information on the distribution of hot water in the subsurface. To conduct the survey, shallow holes, approximately one meter deep, were augered with a small hand-held power auger, at numerous locations throughout the spring area. The hole locations were marked, and after sufficient time had passed for the soil to dissipate the temperature effects induced by drilling, the sites were revisited and temperature measurements made. Additional measurements were taken in and around the lakes and spring orifices by pushing a long, thin temperature probe into the bottom muds and grass mat to a depth of approximately 1 meter. All of the temperature measurements were taken within a three day period during September of 1977.

The measurements were made with a thermistor device built at UGMS in which the resistance across the thermistor is read directly as temperature (°C) on a liquid crystal display, to within .1°C. The thermistor is mounted on the end of the probe which is about 2 meters long.

Results

The results of the shallow ground temperature survey, shown in figure 10, were very useful, and a number of assumptions that had been made on the basis of these data were later confirmed by the drilling of 75-meter (250 ft.) gradient holes. The main features to be noted in figure 10 are:

1. A distinct north-northeast trending zone of high temperatures that is coincident with the the eastern zones. The temperatures reach a maximum of 86°C near the southern end of the zone, but temperatures of 80 to 85°C were measured at other orifices in that zone.



Relative levels of pond surfaces and approximate water elevations in wells in the vicinity of Crystal Hot Springs, Salt Lake County, UT.

Figure II

2. A rapid decrease in temperature with distance to the east of the high temperature zone. The temperatures decrease from 80 to 85°C to less than 20°C over distances commonly less than 100 meters distance from the high temperature zone. The coolest temperatures measured were approximately 12 and 13°C in the southeasternmost corner of the study area.

3. A gradual decrease in ground temperature to the west of the high temperature zone. The 20°C isotherm is commonly 200 to 300 meters west of the high temperature zone.

4. The presence of warm water in numerous spring orifices southwest of the eastern lakes. Temperatures taken in most of these orifices were between 50 and 60°C, but in those that had outlets and flowed, temperatures were as high as 75°C. The majority of these orifices are in a zone that trends east-northeast in the south-central portion of the area.

5. The presence of a number of hot water spring orifices in the large western lake. At least three major orifices exist and others may be present. Their detection, however, was difficult because water depths exceeded 15 m (50 feet) in several portions of the eastern half of the lake.

6. Relatively cool ground temperatures that lie to the north and south of the large western lake. Temperatures in these areas are commonly 17 to 18°C.

Water Chemistry

Analyses from a number of locations in the vicinity of the hot springs are presented in table 1. Temperature pH, conductivity and HCO₃ determinations were done by UGMS personnel in the field. The remaining parameters were determined by the State Health Department laboratory on unacidified samples. All samples were filtered in the field, but the strict sampling procedures outlined by the U.S.G.S. (Presser and Barns, 1974) were not followed when the samples were collected. The analyses in table 1 should be used as indicators of general water chemistry only, and are not suitable for use in geothermometry calculations.

The chemical quality of the thermal water of Crystal Hot Springs is excellent when compared with other low temperature thermal waters along the Wasatch Front. The total dissolved solids content has been used to rank the general water quality of Wasatch Front springs as presented in table 2.

The factors contributing to the anomalously good quality of the thermal waters at Crystal Hot Springs are not fully understood, however, a number of factors could possibly contribute to the observed water chemistry. First, the water recharging the system is snow melt and low in total dissolved solids. Second, the water may move rapidly through the system thereby decreasing the time available for the dissolution of soluble components along the flow path. Third, the material through which the

water flows is not readily soluble. Fourth, the thermal water has not been contaminated with non-thermal brines

LINEAMENTS

The most prominent linear feature on the north flank of the East Traverse range is the base of Steep Mountain (see figure 21 A). Gilbert (1890) and Marsell (1932) did not recognize the plane of Steep Mountain as a fault line scarp, but referred to the feature as a great sea cliff. Slentz (1955), Dolan (1957), and Bullock (1957) present evidence that supports the theory that the north face of Steep Mountain is a fault line scarp. Bullock (1957) also suggests that a second scarp coincides with the Provo shoreline at an elevation of 1463 m (4,800 feet).

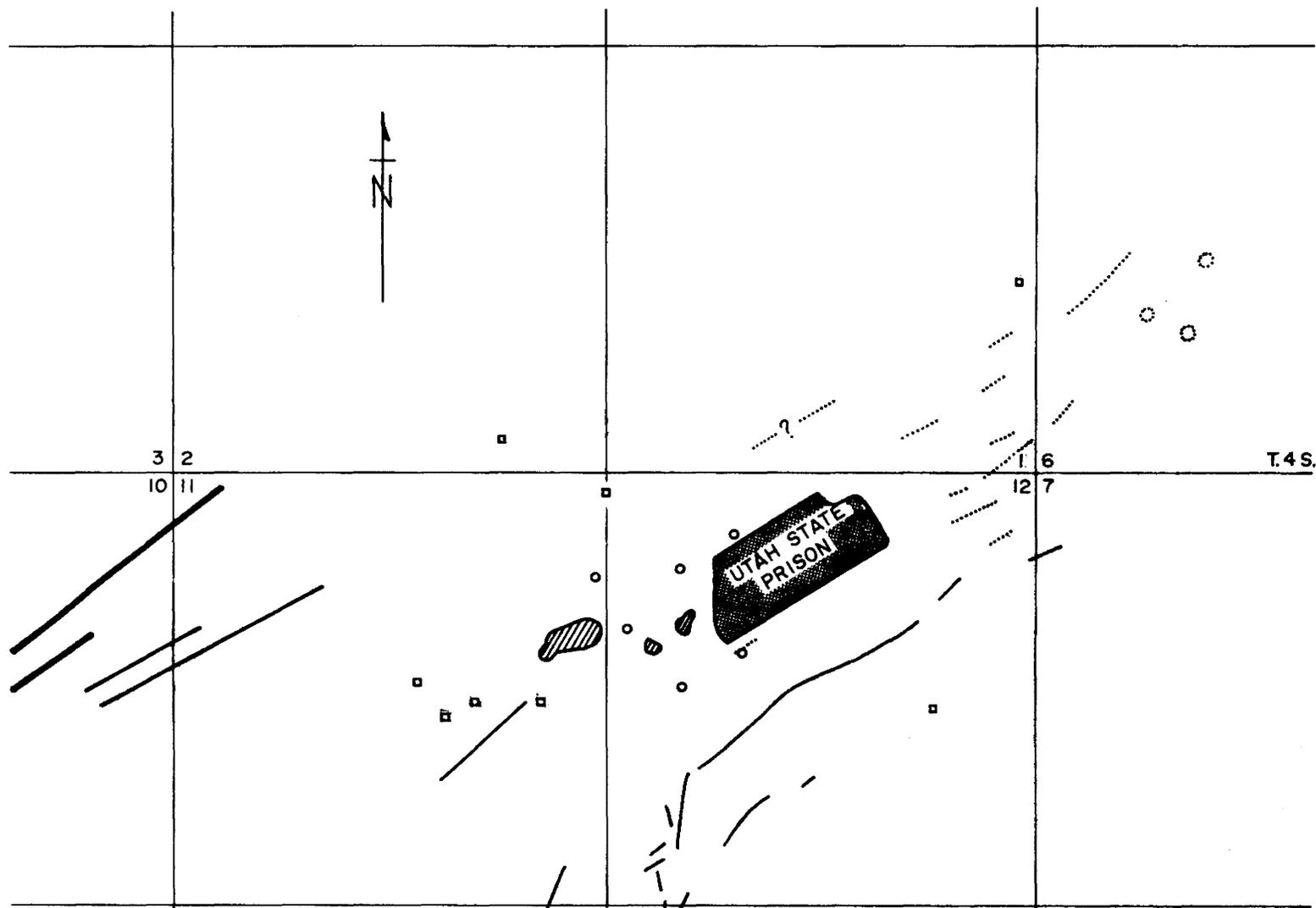
Structures buried under Quaternary valley fill often have subtle expressions at the surface of the valley fill. In figure 12 two sets of lineament data taken from aerial photography are portrayed: 1) lineaments reported by Cliff, et. al. (1970), and 2) leached soil lineations observed by UGMS personnel.

Cliff, et. al. (1970) used low sun angle photography to identify scarps and tilted ground surfaces related to faulting or ground movements. Lineaments were divided into three classes based on the level of certainty that the lineaments were controlled by faulting as follows:

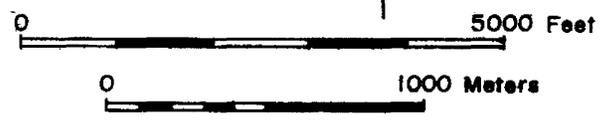
- CLASS I - Prominent or obvious fault, or very fresh fault related feature
- CLASS II - Probable fault or rupture, or fault showing a lack of recent activity.
- CLASS III - Possible fault or rupture.

Class I and II lineaments in figure 12 are beyond the area covered by the special low sun angle photography used for the investigation but the scarps are visible on standard aerial photography as vertical displacements and linear features in alluvium in the vicinity of the Jordan River channel. These scarps strike at N40°E, roughly paralleling the mountain front below an elevation of 1402 m (4600 feet). Above 1402 m (4600 feet) there are a great number of class III lineaments that closely parallel the Provo and Bonneville shorelines. There are two sets of class III lineaments in figure 12: 1) those striking northeast that are related to the main range front structural trend; and 2) a group of short lineaments that, as a unit, strike north-northeast and are possibly related to north-northeast striking features present in the subsurface.

The soil lineaments in figure 12 can be seen on standard areal photography as light colored soil patches having a very straight, well defined northern edge and irregular boundaries on the south. Soil within the light patches is enriched with calcium carbonate with respect to the surrounding soil.



- Explanation**
- Spring associated lakes
 - Lineations (Woodward and Clyde, 1970) - below 4,600'
 - Class I
 - Class II
 - Class III
 - Soil lineaments
 - Quartzite outcrops in valley fill
 - Water wells
 - Gradient holes



**Structural Trends at Crystal Hot Springs
Salt Lake County, Utah**

Figure 12

Table 1. Water analyses of well and spring water in the vicinity of Crystal Hot Springs

Owner or Name	Temp.	Depth	Date of Collection	mg/l					HCO ₃	SO ₄	Cl	T D S	Cond. mmho	pH
				SiO ₂	Ca	Mg	Na	K						
Crystal Hot Springs eastern ponds	61.6 °C		6/22/78	66	128	34	325	70	230	74	590	1,462	2.4 x 10 ³	5.9
State Forestry Test Well	62. °C	280	6/21/78	59	136	39	380	70	260	71	685	1,660	3.0 x 10 ³	6.25
Water Well Hall	39. °C	236	6/21/78	30	132	34	220	45	260	52	530	1,304	2.7 x 10 ³	6.4
Water Well -Lear	18. °C	200	6/22/78	26	88	49	115	8	210	200	160	842	1.36 x 10 ³	6.8
Water Well Fitzgerald	16.1 °C	167	6/29/78	45	82	55	150	20	210	280	210	1,052	1.65 x 10 ³	7.16
Water Well USP	16.2 °C	800	6/29/78	20	45	23	22	2	150	29	36	288	5.1 x 10 ²	7.3
Camp Williams Warm Spring	23.5 °C		6/30/78	24	54	29	25	5	170	41	58	372	5.6 x 10 ²	7.45

23.

Table 2. Approximate total dissolved solids and maximum reported temperatures at selected Wasatch Front thermal springs.

Spring	Approximate TDS (mg/l) *	Maximum reported Temperature
Crystal	1,500	86 °C (187 °F)
Saratoga	1,500	44 °C (111 °F)
Udy	7,900	54 °C (121 °F)
Wasatch	8,600	42 °C (108 °F)
Beck	13,700	55 °C (132 °F)
Utah	29,200	62 °C (144 °F)
Crystal (Madsen)	42,900	57 °C (135 °F)

*From Mundorff (1970)

Although the origin of the lineations is still in question, a tentative hypothesis is that the light soil patches are concentrations of calcium carbonate deposited in small sag ponds associated with buried range front structures. Minor topographic lows were not noted to occur with the light soil patches, but years of farming may have masked the very slight depressions.

The quartzite mounds in figure 12 are along the major structural trend, and are anomalous in that they are totally surrounded by valley fill. The water well 457 m (1500 feet) north-northwest of the westernmost outcrop encountered quartzite at a depth of 91 m (300 feet).

Geophysical Investigations

Magnetic Surveys

Two types of ground magnetic surveys were undertaken at the Crystal Hot Spring resource using an E. J. Sharpe, Fluxgate vertical field magnetometer (Model no. MF-1T-100). First, a detailed survey in the vicinity of the springs was made in which most of the shallow ground temperature grid stations were occupied with the magnetometer. Readings at any given station were quite variable due to problems with the magnetometer, and any minor magnetic variations were not identifiable. Second, two one-mile traverses X-X' and Y-Y' shown in figure 13 were run to determine the position of the magnetic high shown on the state magnetic map (Zietz, et.al. 1976) relative to the hot spring system. As the profiles are not tied into a magnetic base station of known value, the readings are only relative, and diurnal magnetic variations have not been removed. The most prominent feature in profile X-X' is the large magnetic anomaly at the northern end of the area. The anomaly is very steep on the southern flank, increasing sharply over a very low background value, to the south. The profile is interpreted as indicating that material of high magnetic susceptibility in the subsurface is positioned adjacent to material of very low magnetic susceptibility. The north end of profile Y-Y' has a similar but less intensive anomaly and the slope of the southern flank is not as steep nor the anomaly as intense as that seen in profile no 1. The anomaly at the south end of profile Y-Y' is presently unexplained, but may represent a small patch of volcanic material on the Oquirrh Formation.

Aeromagnetic Survey: A total intensity aeromagnetic map flown by the U. S. G. S., but contoured by ASARCO (1954), was provided to the UGMS by ASARCO after profiles X-X' and Y-Y' had been run. A portion of the ASARCO map is reproduced in figure 14.

The anomaly, as depicted on figure 14, is elongated in an east-west direction, and roughly parallels the northern flank of the East Traverse Mountains. The most intense portion of the anomaly is roughly triangular in shape and is bounded by the 1,400 gamma contour. The springs and the State Prison are located on the southern flank of the anomaly. Within the area of the anomaly defined by

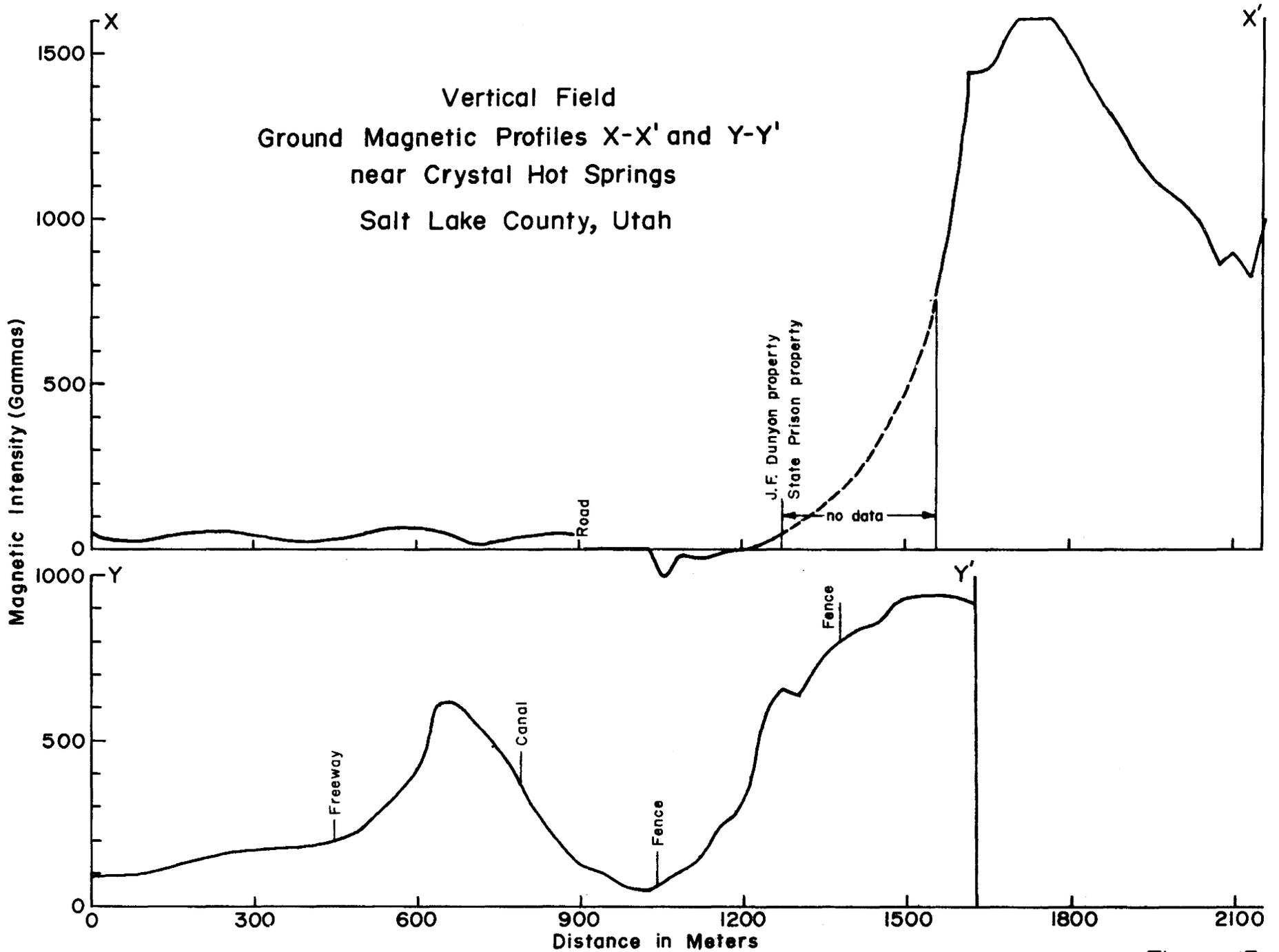
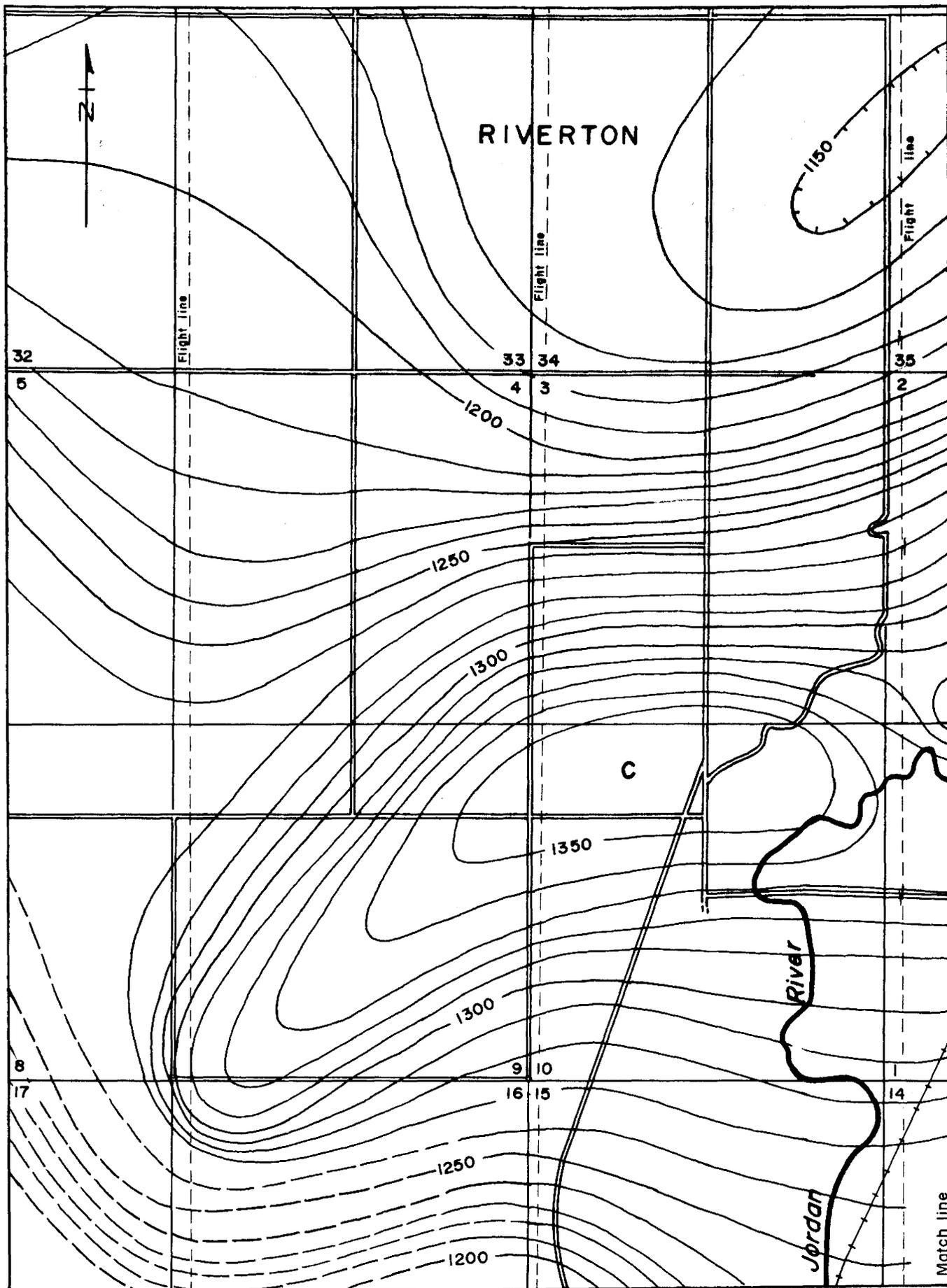


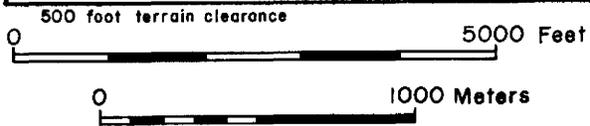
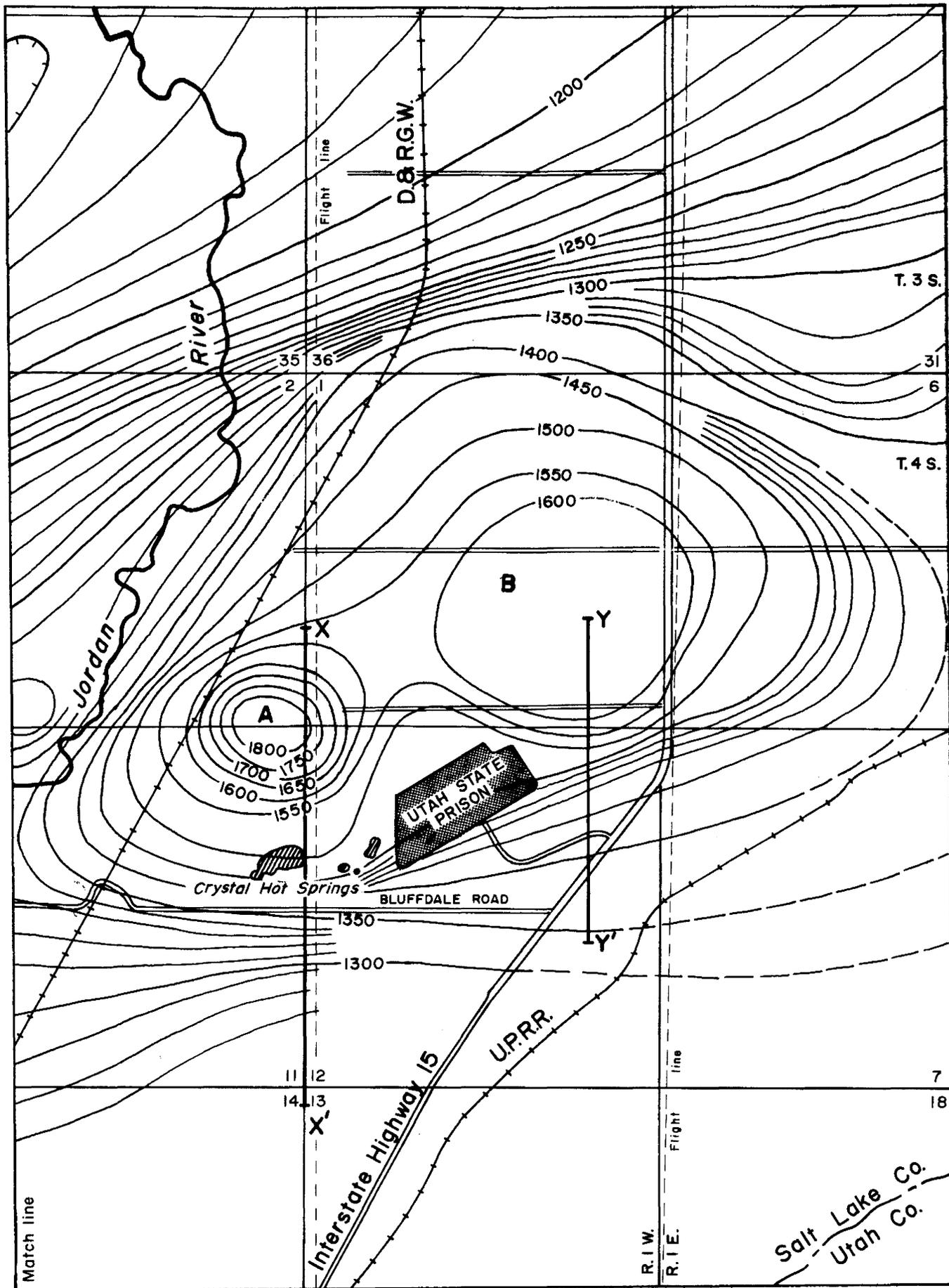
Figure 13



500 foot terrain clearance

Aeromagnetics in Vicinity of Crystal Hot Springs

Figure 14a



Adapted from A.S. & R. Co. compilation of U.S.G.S. data, A.S. & R. Co. (1954)

Figure 14b

the 1,400 gamma contour are two roughly circular areas. The western portion ("A" in figure 14) is intense, and relatively sharp as compared to the less intense and broad eastern portion ("B" in figure 14). Just west of the Jordan River is a less intense portion of the total anomaly ("C" in figure 14) with closure at 1,340 gammas. This portion is separated from the magnetic high to the north of the springs by a slight depression in the intensity. The western edge of the anomaly is steep and linear.

ASARCO targeted and drilled the "A" portion of the anomaly to determine if the buried body responsible for the anomaly was mineralized. The location of the drill hole is plotted in figure 16; the log of the hole is presented in Appendix A. At a depth of 113 m (370 feet), an andesite porphyry containing approximately 2% magnetite was encountered; the hole continued in andesite prophyry to a total depth of 287 m (940 feet), mineralization of commercial value was not found.

Magnetics Summary: Magnetic surveys have provided valuable information on the distribution of magnetic materials in the subsurface, and the location of subsurface structures. In the study area, an andesite porphyry with high magnetic susceptibility is present on the downthrown side of normal faults just north of the spring system, and has been faulted against materials of low magnetic susceptibility. Additionally, normal faults in the material of high magnetic susceptibility, having vertical displacement, are also discernable. The differences in the shape and intensity of magnetic anomalies A, B, and C are likely to be attributed to vertical displacement of the andesite porphyry to varying depths across normal faults.

Gravity Surveys

The only gravity data available for the Traverse Mountains area are those published by Cook and Berg (1961). The Traverse Mountains are coincident with a regional gravity high that separates the Jordan Valley graben to the north from the Utah Valley graben to the south (figure 15). Although only a few gravity stations are present in the immediate vicinity of the springs, the isobars are shifted valleyward in the vicinity of the hot springs, thus putting the hot springs on the local gravity high, on the southern flank of the Jordan Valley graben.

DRILL HOLE DATA

Holes of Opportunity

A number of water wells exist in the vicinity of the hot springs, and have provided data in areas where gradient holes were not drilled by UGMS. The holes referred to as Lee, Hall and U. S. P. (figure 16), (Utah State Prison) were open at the beginning of the investigation. The ASARCO exploration

hole was cleaned to a depth of 42 m by UGMS at the time the gradient holes were drilled. The Lear hole was drilled as a water well at the time gradient hole drilling was proceeding, but independent of the UGMS project. Lithologic information for water wells, when available, is taken from driller logs, and is presented in Appendix A.

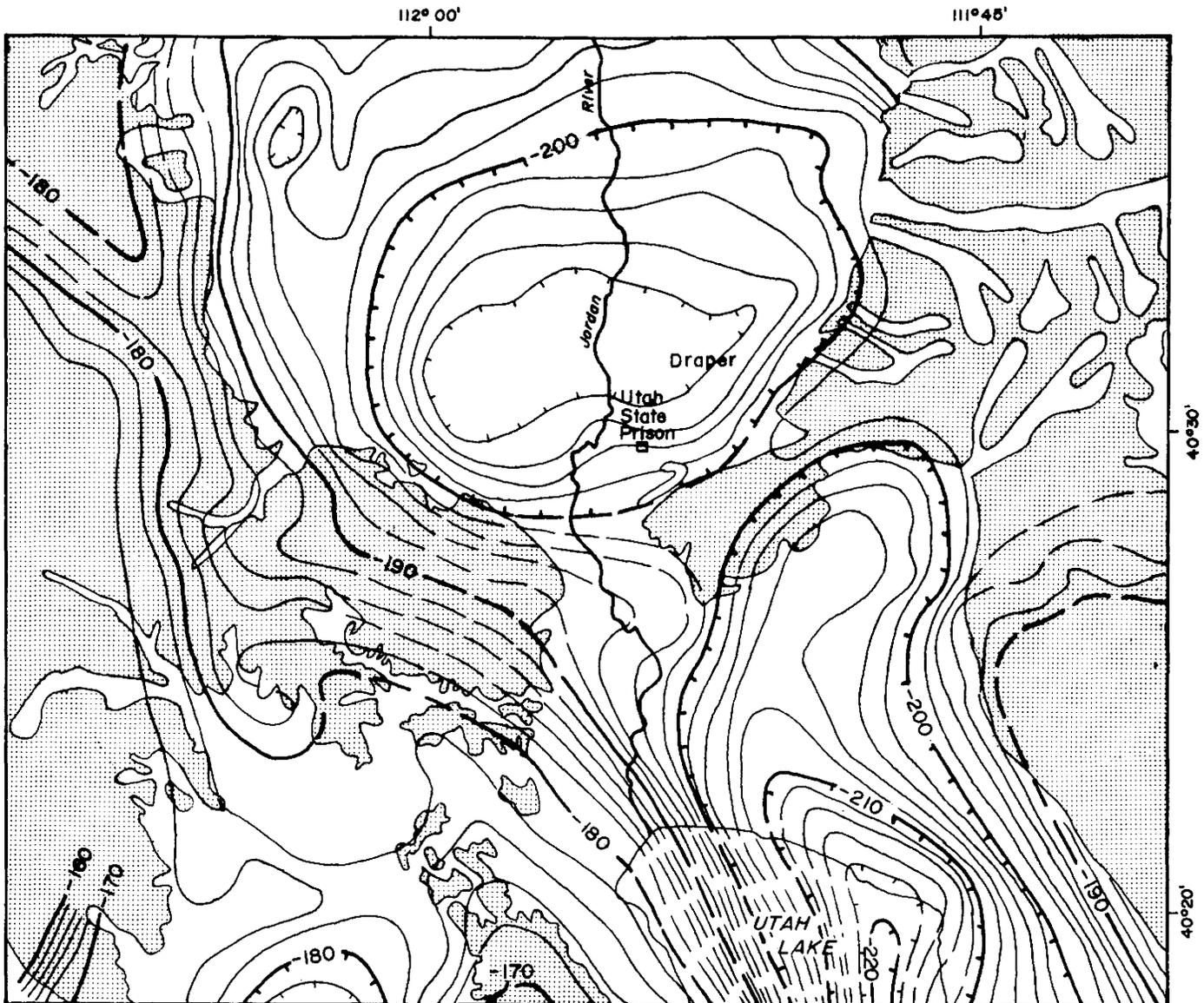
Gradient Holes

The information presented in previous sections was used to site six geothermal gradient holes in and around the Crystal Hot Spring system. The drilling was done by K. O. Burt, of Springville, Utah, who began drilling on February 17, 1978, and finished on March 21, 1978. Drilling was done with a rotary rig, and holes were completed to depths that range from 61 m to 85 m (200 to 280 feet). Each hole was spudded with air then advanced to the desired depth using mud. Upon completion of the drilling, a one inch black iron pipe, capped at the bottom, was run to the total depth of the hole. The hole was then back-filled with cuttings, where possible, and the top 3 m (10 feet) filled with concrete. When artesian conditions were encountered, the holes were grouted from total depth to the surface.

The six gradient holes were sited to yield a maximum of information pertaining to the spring system and to test the hypotheses made after conducting the shallow ground temperature survey. Holes (C, D, E) were drilled across the surface expression of the springs along a line that strikes to the northwest (figure 16). Holes (B, F) were drilled to the east of the springs where ground temperatures had been found to decrease rapidly with distance from the eastern lakes. Hole (A) was drilled near what was believed to be the possible intersection of two faults. A number of existing water wells (holes of opportunity) to the south and west of the system were used to fill in data on geology and temperatures present in those areas. Subsequent to gradient hole drilling by UGMS, the Division of State Forestry drilled a geothermal production well for the purpose of space heating a greenhouse. The Forestry well was drilled between gradient holes A and D, and is referred to as SF-1.

The gradient holes were logged and the cuttings sampled as drilling proceeded. The samples were divided into two portions, one portion was dried and preserved as it was taken, and the second portion was washed and saved for analysis. These samples are stored in the UGMS sample library. Lithologic logs of the holes are presented in Appendix A.

The gradient hole drilling program has provided subsurface geologic, hydrologic, and temperature information unattainable by any indirect method. The nature, thickness, and lateral extent of unconsolidated material; as well as the nature, distribution and depth to consolidated material are a number of geologic parameters that have been determined from the drilling program.

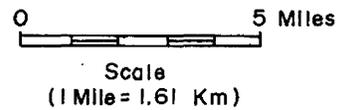


For control, see original reference.

EXPLANATION

-  Bedrock
-  Alluvium (including TQu)
-  Gravity contour—dashed where inferred. Contour interval 2 milligals. Bouguer anomaly values.

Adapted from Plate 13 of Cook and Berg, 1961



Bouguer Gravity Anomaly for the Central Wasatch Front, Utah

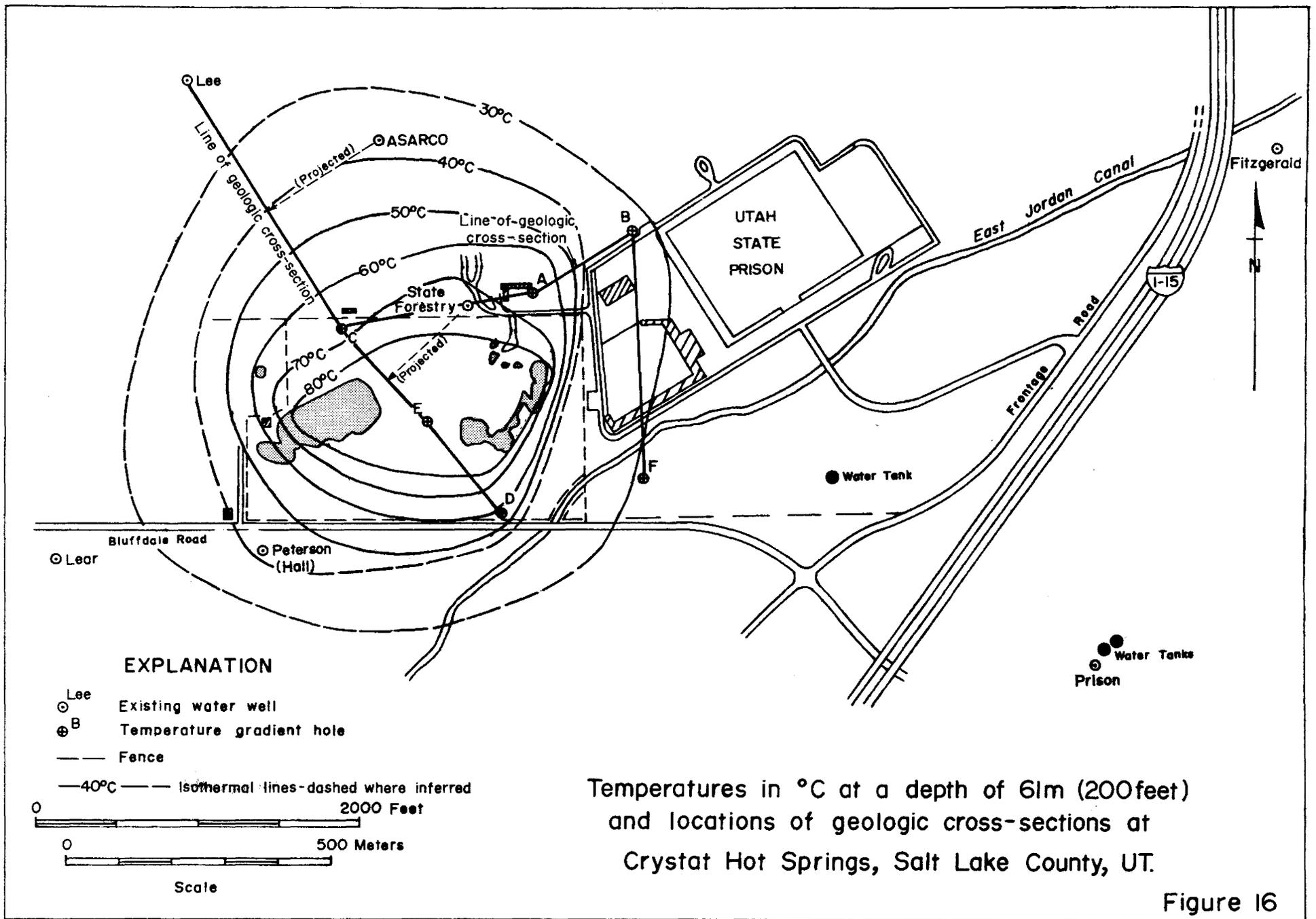


Figure 16

Geology

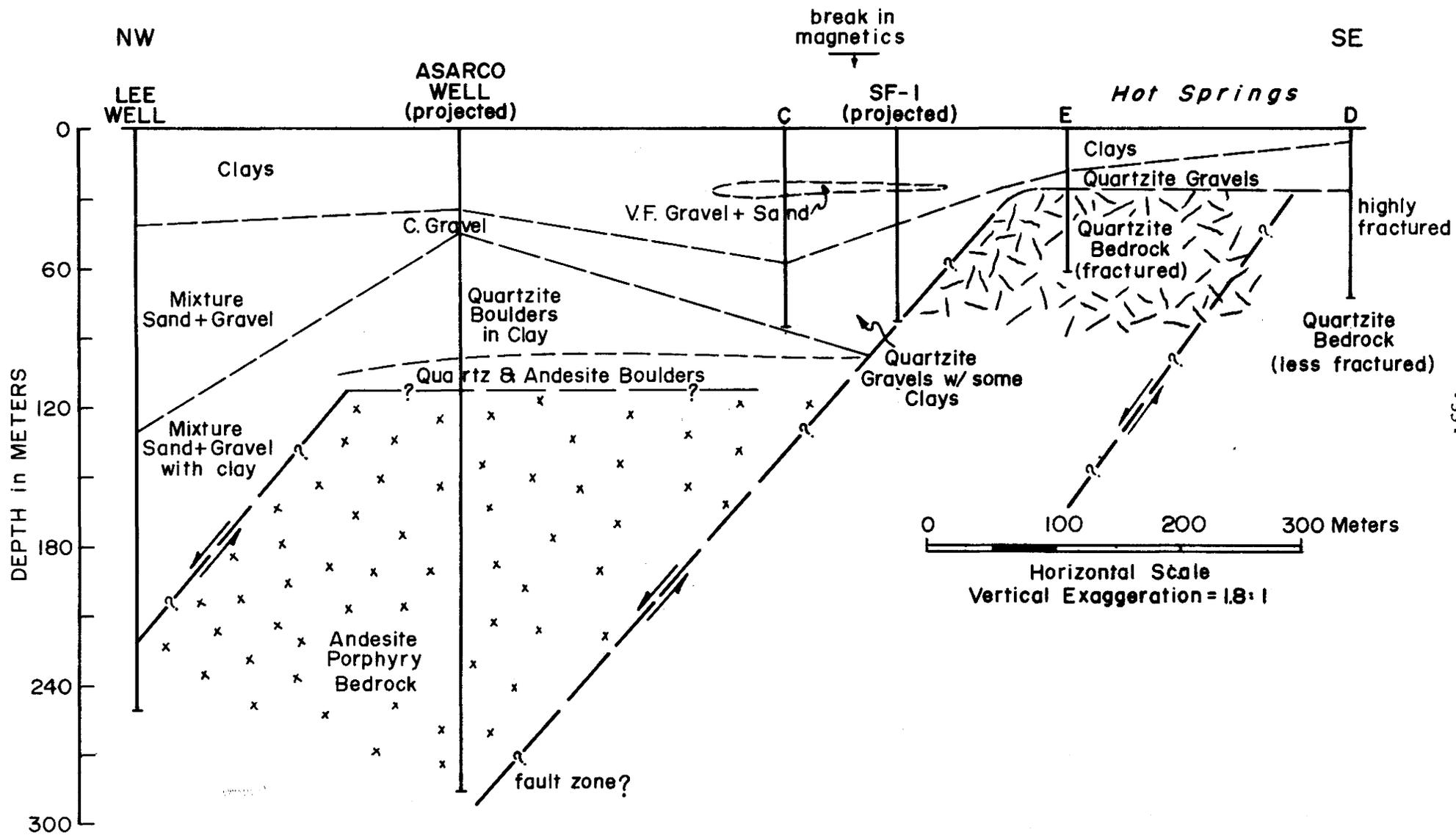
By using generalized forms of lithologic logs (Appendix A), cross-sections through the area of the springs have been prepared and are presented in figures 17 and 18. Cross-section Lee-D in figure 17 shows a faulted bedrock surface mantled by unconsolidated materials. At the surface, a variable thickness of clay overlies more permeable sands and gravels. The clays are lake clays and contain variable but small amounts of sand. Interbedded in the clays are lenses of sand and sandy gravel with clay that reach a maximum thickness of less than 6 m (20 feet); the clay content appears to decrease with depth in some holes. In the immediate vicinity of the springs (holes D and E) a clean quartzite gravel overlies the fractured quartzite bedrock. Northwest of the springs, the clay content in the quartzite gravels increases, and further west, the gravels are a mixture of sand and well rounded gravel and cobble. Over the downthrown block (figure 17), the Lee and ASARCO holes penetrated additional unconsolidated material consisting of sand and gravel with clay and quartzite boulders in clay.

The bedrock surface in figure 17 was determined by using the drill hole data and the magnetic data discussed above. The main features of the cross-section through the bedrock are: 1) the normal step faulting generally associated with Basin and Range structure, 2) the fractured quartzite on the up-thrown side of the southernmost fault, and 3) the andesite porphyry, of high magnetic susceptibility, on the downthrown block of the southernmost fault. Although other interpretations of the data are possible, this cross-section is the simplest cross-section that could be drawn with the available information.

Figure 18 is the cross-section along C-F in figure 16. Beneath the zone of clay at the surface, the unconsolidated materials in holes B and F were significantly different from the unconsolidated materials to the west. The gravels encountered in holes B and F contained significantly more clay and occasional boulders that were not present under the hot springs. The fault indicated in cross-section C-F is based on three lines of evidence: 1) bedrock was not encountered at the depths close to those in holes D and E, 2) the saddle in the aeromagnetic anomaly (figure 14), and 3) the rapid decrease in ground temperatures east of the easternmost lakes (figure 10).

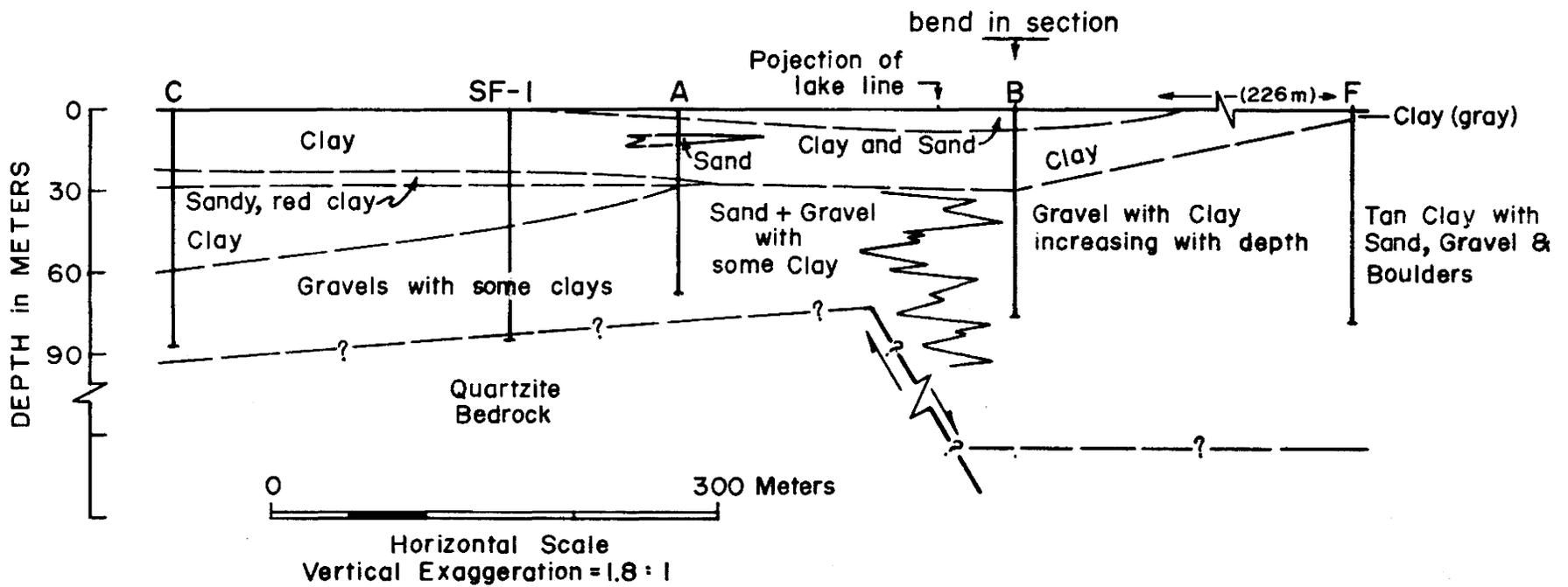
Temperatures

After the gradient holes were completed, they were allowed to equilibrate before temperature gradients were measured. Measurements were made by lowering a thermistor into the one inch pipe and taking readings every 1.5 m (5 feet). The instrument used for the temperature measurements is a thermistor type device (accurate to $.05^{\circ}\text{C}$) manufactured by Fluid Dynamics Corporation of Golden,



NW-SE Geologic Cross-Section through Crystal Hot Springs
Salt Lake County, Utah

Figure 17



Geologic Cross-Section at Crystal Hot Springs
Salt Lake County, Utah

Figure 18

Colorado. The temperature values obtained from the device are initially read as resistance values which are then converted through a conversion chart to temperature in °C.

The results of the temperature measurements from the gradient holes at Crystal Hot Springs are presented in figure 19. Two sets of curves are shown on this data set. Holes A, C, D, and E all have maximum temperatures greater than 60°C, very steep gradients in the upper 20 m (65 feet), and all the curves are somewhat irregular in shape. Holes F and B have maximum temperatures of 35°C (95°F) or less, and have nearly linear gradients from top to bottom.

In general, the steep gradients in the upper portions of holes A, C, D, and E correlate with the predominantly clay lithologies logged at the top of each hole. Through the clay, a thermal insulator, the temperature increases rapidly with depth to the temperature of water in the underlying relatively permeable material saturated with thermal water. From that point, to the total depth of the hole, each curve is distinctly different.

Hole A. The gradient in the lower portion of hole A is somewhat irregular, but when a straight line is fitted to the curve, a gradient of 254°C/km is obtained. The irregularities in the temperature curve correlate with a complex series of sands and gravels with some clay.

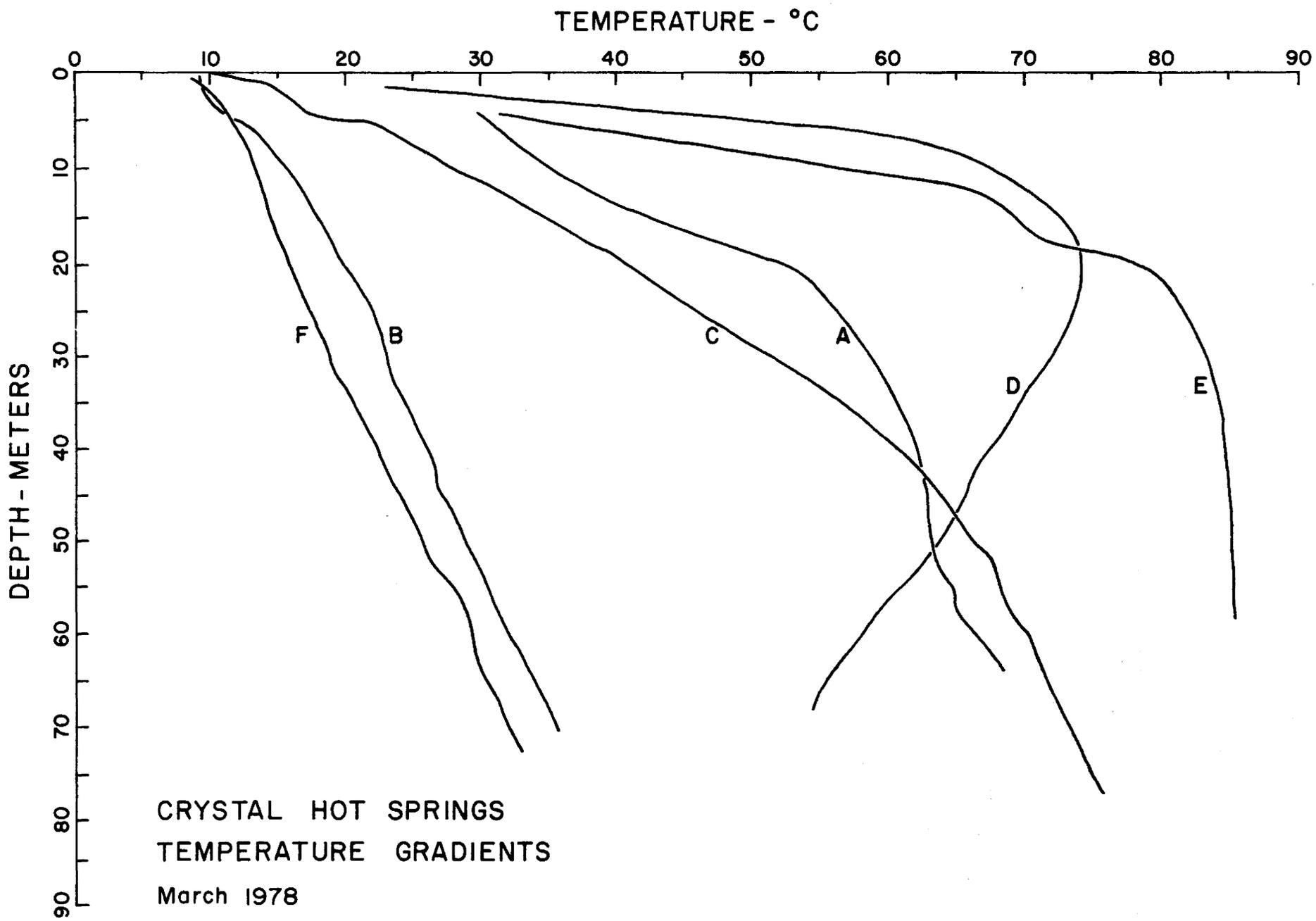
Hole C. The gradient in hole C constantly decreases with depth; the curve is smooth, but an inflection point occurs at approximately 53 m (175 feet). Beyond this point the gradient decreases more slowly and when fitted with a straight line, the lower part of the curve has an approximate gradient of 325°C/km.

Hole D. Temperatures in hole D increase to a maximum of 74.2°C(165°F) at a depth of 20 m (65 feet). From this depth to the total depth of the hole, the gradient in the hole has a steep negative gradient of -459°C/km.

Hole E. The gradient in hole E is approximately 4,300°C/km through the clay at the surface, but then shows a decrease as a straight line through the bottom portion of the curve represents a gradient of 32°C/km. Had this hole continued, it is likely that the temperature gradient may have become isothermal.

Hot geothermal water was not present in holes B and F, and the elevated temperatures in these holes is a result of thermal conduction from below. The gradient in both holes is relatively constant, and the curves generally parallel each other. A straight line through the curve for hole B represents a gradient at 329°C/km, for gradient hole F, the gradient is 325°C/km.

Gradients were also measured in four water wells and the upper portion of the ASARCO ex-



CRYSTAL HOT SPRINGS
TEMPERATURE GRADIENTS
March 1978

Figure 19

ploration hole (figure 20). Straight lines fitted through the lower portions of each of the temperature curves yield the following gradients.

C/WW-ASARCO	150°C/km
C/WW-Lee	93°C/km
C/WW-Lear	90°C/km
C/WW-Hall	98°C/km
C/WW-USP	13°C/km

The Lee, Lear, and Hall wells have gradients from 90 to 98°C/km, however, this value is not representative of the regional geothermal gradient. All of the holes mentioned are being influenced by the hot Spring System; possibly by the lateral flow of warm water in aquifers below the depths penetrated by these holes. The USP hole was completed in an artesian cold water aquifer and the thermal gradient is also not representative of the regional geothermal gradient.

The map of temperatures at 61 m (200 feet) in figure 16 illustrates the boundaries presently known to limit the surface repression of the hot spring system. The rapid changes in temperature on the south and east edges of the system are inferred to coincide with the structures discussed previously. The gradual decrease in temperature to the north and west reflects the northwestward flow of warm groundwater in near surface aquifers.

Pump Test of C/WW-SF

On November 7, 1978, a pump test was run on the geothermal test hole drilled by the State Forestry Service in order to obtain data on well yield and aquifer characteristics. Results of the test were modeled by Christian Smith of the University of Utah Research Institute/Earth Science Lab. His discussion of the results is presented in Appendix B. In general, the pump test indicated that the unconsolidated aquifer in which the well is completed is of low transmissivity, and that 30 gpm is the maximum yield to be expected from the well. Pumping the well at 30 gpm over an extended period of time should not have a significant effect upon the natural regime of the springs.

SUMMARY OF THE STRUCTURES IN THE VICINITY OF CRYSTAL HOT SPRINGS AND THE JORDAN NARROWS

Crystal Hot Springs

In previous sections of this report considerable evidence has been presented indicating the structural complexity of the area surrounding Crystal Hot Springs. Using the available evidence, a summary of the structural elements for which the best evidence exists is presented in figure 21. Other structures exist within this area, but confidence in their locations is limited at the present time.

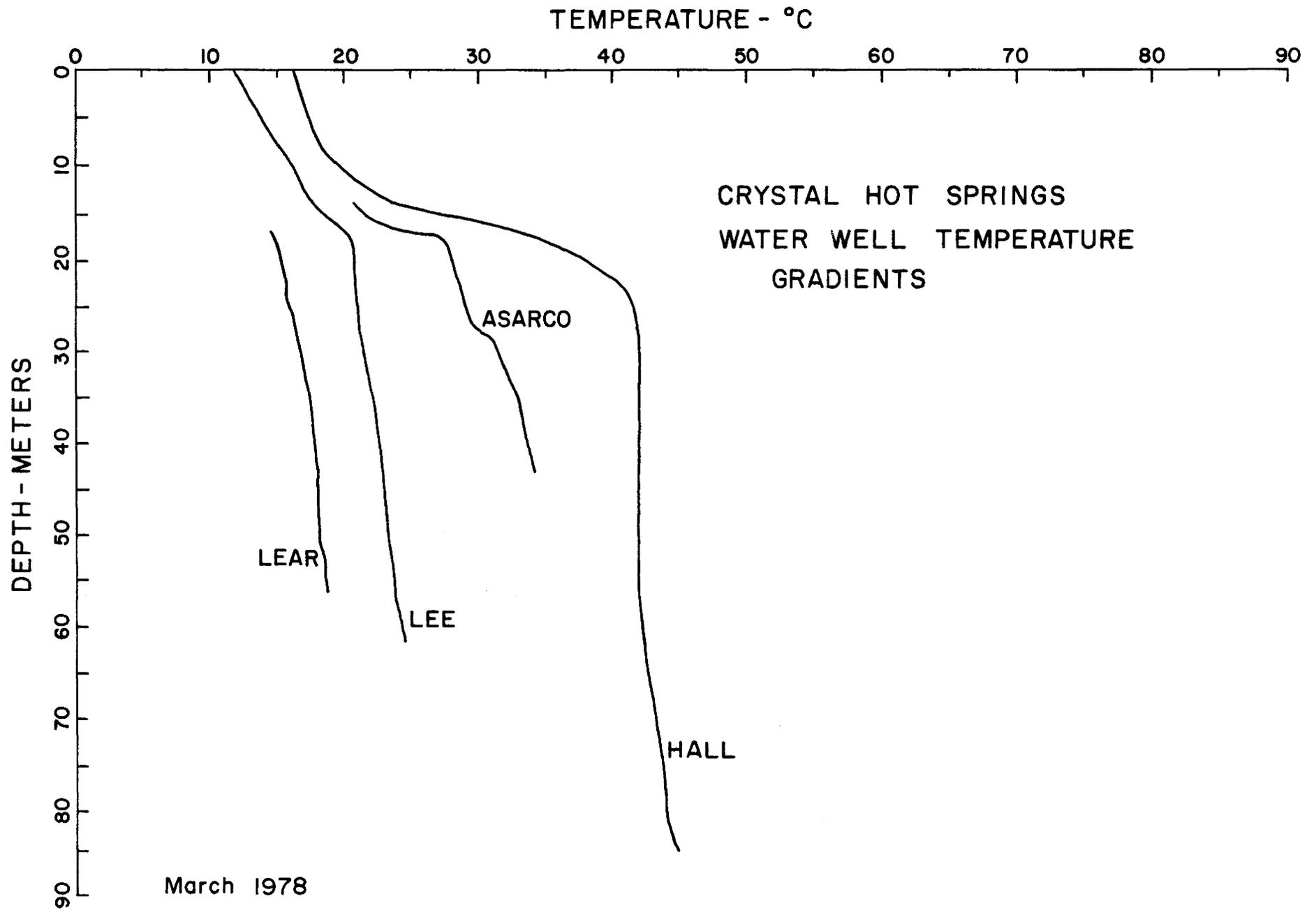


Figure 20

The following is a brief discussion of the structural elements in figure 21, and the possible resource controlling influences of each of three structural trends: northeast, north-northeast, and northwest.

The most prominent fracture set is a series of normal range front faults that strike northeastward and dip northwestward toward the Jordan Valley graben (figure 21 A). The Steep Mountain fault, and the fault coincident with the Provo shoreline are two of the range front faults that are exposed at the surface. Several other faults trending northeast are present beneath the valley fill. A range front fault having over 90 m (300 feet) of bedrock relief across the fault is present just north of the State Prison. Well data, aeromagnetic data, and a second class lineament, all discussed earlier, define the location of this fault.

The second set of fractures strike north-northeast. This trend was first noticed at the eastern edge of the spring system (figure 10) and repeats itself a number of times on the aeromagnetic surface. Based on the difference in the intensity and shape of the A and B portions (figure 14) of the aeromagnetics anomaly, and the difference in the depth of bedrock, as determined by gradient hole drilling, the movement on the fault coincident with the eastern springs appears to be down to the east-southeast. If the fault is normal, the dip of the fault plane is to the east-southeast. The total displacement on the fault is unknown but the relief on the bedrock surface is estimated to be on the order of 90 to 120 m (300 to 400 feet).

The third set of structures trends roughly northwest and is best expressed by the fault that bounds the eastern edge of the Jordan Narrows graben (figure 21 B). A second fault with a northwest trend is present near Rideout quarry and displaces the Provo shoreline fault (figure 21 A).

The northeast trending faults in the vicinity of the springs appear to limit the expression of the geothermal resource on both the northwest and southeast and may actually define the limits of the system at depth. The highly fractured quartzite in which the hot water is found in the near surface may be effectively sealed to the northwest by the andesite porphyry faulted against the quartzite and to the southeast by less fractured quartzite. Evidence for the system being bound on the southeast by a fault is present in the temperature gradient taken in hole D (figure 19). The quartzite encountered in hole D was very similar to that encountered in hole E, however, the gradient in hole D reverses, indicating the absence of hot water in the quartzite penetrated by the hole.

Evidence that the fault which bounds the eastern edge of the spring system dips east-southeast, and is the conduit for the movement of hot water to the near surface, is found in the gradients obtained from holes B and F (figure 19). As discussed above, the gradients in B and F indicate conductive heat flow, and the absence of hot water moving through the material penetrated by the holes. The

gradients for the holes are very high, and indicate the presence of abnormally high temperatures at depth. Projection of the gradients observed in holes Band F to the maximum temperature observed at Crystal Hot Springs of 86°C places a possible fault plane transporting hot water, at approximately 245 m (800 feet) beneath the surface in the vicinity of the holes. However, projection of gradient data is very risky, and the observed gradients may be the result of hot water recharging into near surface unconsolidated aquifers at depths much less than 245 m (800 feet). Further investigations planned under the PON awarded to the State of Utah by DOE will provide the data needed to determine the subsurface conditions.

At the present time there is little evidence to indicate that the northwest trending structures have any influence on the expression of the resource. Further investigation will be necessary to determine whether or not these fractures influence the movement of water into the near subsurface.

Jordan Narrows

There does not appear to be any large structural or stratigraphic discontinuity between the East and West Traverse Ranges (Marsell, 1932), but the Jordan Narrows appears to be a structurally complex graben. The graben strikes northwest and is bound on the northeast and west by normal faults. Northeast striking faults cut perpendicular to the graben trend.

Evidence for the faults bounding the Jordan Narrows graben includes:

- 1) Major pre-pleistocene displacement along the north-south striking fault mapped just west of Camp Williams. Slentz (1955) indicates that the Jordan Narrows unit of the Salt Lake group is faulted down against Paleozoic rocks.

- 2) Major displacements on the bedrock surface buried beneath the Lake Bonneville spit just east of the Jordan Narrows (figure 21 B). The displacement was detected in an electrical resistivity sounding profile (figure 22) carried out by Zohdy and Jackson (1969). Depth to bedrock in water wells on strike with the westernmost structure indicate the structure may extend northward, possibly as far north as the linear bluff south of Bluffdale road (figure 21 A).

Slentz (1955) mapped a series of northeast trending structures in the Jordan Narrows that he indicates as being branches of the Steep Mountain scarp in the East Traverse Range. In figure 21 B these faults are shown as unconnected sub-parallel faults but they are undoubtedly related to the range front faults in some undetermined manner. These faults displace all the units assigned to the Tertiary Salt Lake group except the Travertine unit.

Although no fault has been indicated in figure 21 B the travertine deposit in the vicinity of the

Camp Williams warm spring, (C-4-1)23bcc, and the large travertine deposit on the west flank of the West Traverse Range, (C-4-1)27bb, are on strike with the fault indicated at an elevation of 4800 feet on the East Traverse Range. The fault may extend across the Jordan River Valley and may have influenced the movement of thermal water during the Tertiary.

THE CRYSTAL HOT SPRING GEOTHERMAL SYSTEM

System Recharge

The water in the Crystal Hot Springs system is meteoric in origin, and the recharge area for the elements carrying the water to depth is undoubtedly the adjacent Wasatch Range. Two elements are likely to be responsible for transporting the water to depth: 1) faults, and fractures or 2) aquifers, or some combination of the two. Since the exposed area of a fault or fault zone may not be extensive enough to provide an adequate recharge area, it can be hypothesized that steeply dipping aquifers in the Wasatch Range are recharged by snow melt and rainfall.

Heat Source

The Crystal Hot Springs geothermal system is a fault controlled, convective system in which meteoric water circulates to depth and is heated by the ambient temperature of the rocks at depth. Within the Basin and Range Province, heat flow is relatively high and the thermal gradient, or change in temperature with depth is normally about 32°C/km. Therefore, water entering the system at the average annual air temperature of 10°C must circulate to depths of approximately 2.5 km (1.55 miles) in order to obtain the maximum observed temperature of 86°C. If some loss of fluid temperature is assumed to occur by mixing or by conduction to wall rock as the water ascends to the surface, then the water may circulate to greater depths. At depth, the heated water enters zones of high vertical permeability associated with faults and quickly returns to the surface.

The heat source for the water at Crystal Hot Springs is not believed to be the cooling of igneous rock at depth. The Little Cottonwood stock, the youngest dated intrusive body in the region, has been dated at between 24 and 31 million years in age while andesite intrusives of the Traverse Ranges have been dated at 37 million years of age (Crittenden, et. al. 1973). Theoretical cooling models developed by Smith and Shaw (1978) tend to support the theory that even the largest intrusive bodies no longer act as heat sources after 10 million years of the last phase of intrusion.

Springs

The shallow ground temperature survey was one of the first activities undertaken by UGMS at

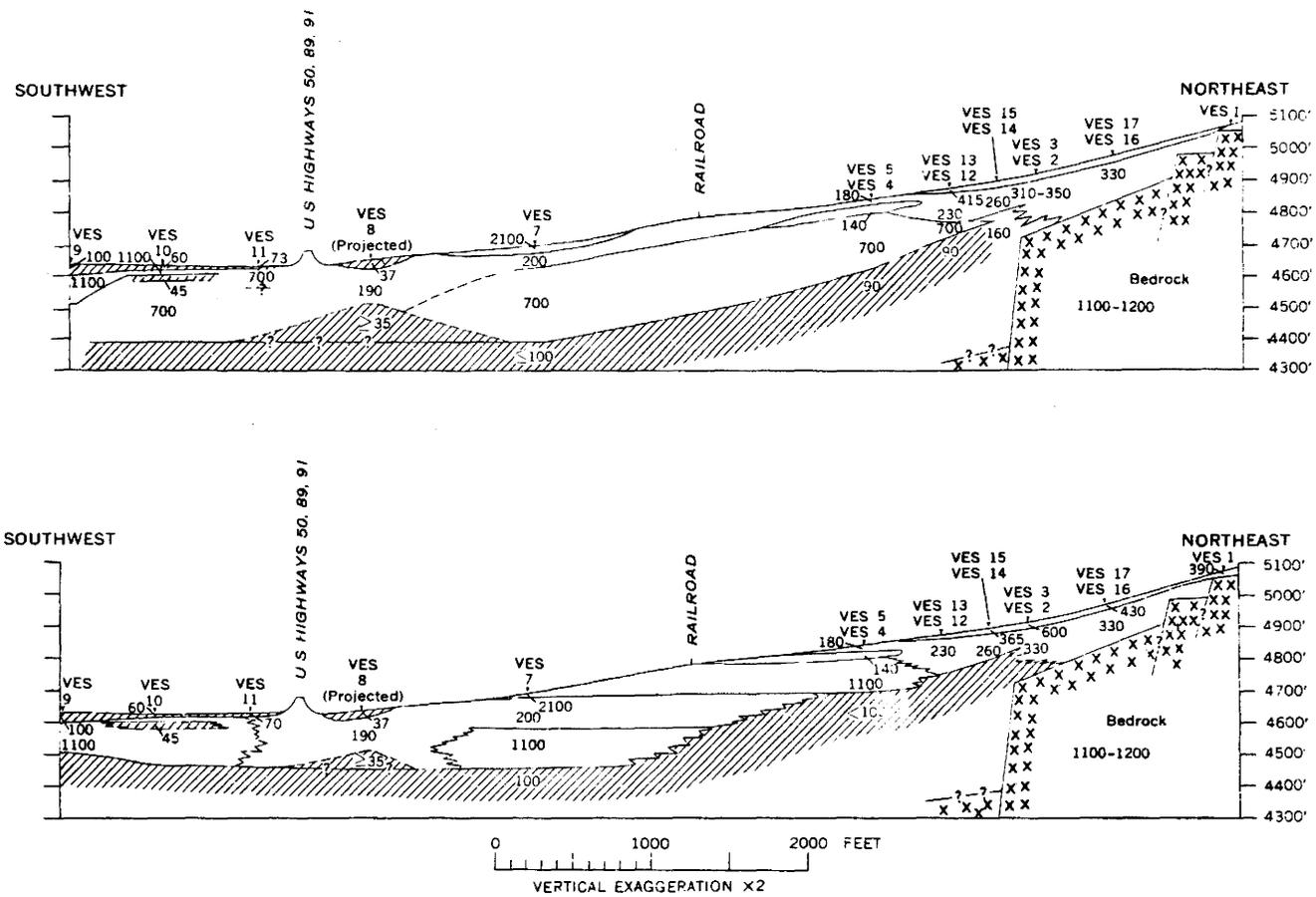


Figure 22. Two equivalent cross sections based on different interpretations of vertical electrical sounding (VES) curves. Numbers designate possible values, in ohm-meters, of true resistivity. Line pattern, low resistivity; stipple, high resistivity. Location of sounding stations shown on figure 1. Profiles shown to illustrate normal faulting in the Jordan Narrows. For explanation of resistivity data see Zohdy and Jackson, 1969.

Crystal Hot Springs. The data from the survey yielded the first indication that structures controlled the resource expression, and was a valuable beginning to the exploration program. The gradient holes that were sited on basis of the results of the shallow temperature survey, and provided information that helped to explain the observed shallow ground temperatures. The following is a description of the near surface portion of the spring system.

As discussed previously, the prominent north-northeast trending zone of high ground temperatures associated with the eastern ponds is coincident with a fault bounding the eastern edge of the spring system. The ground temperatures to the east of the zone decrease rapidly with distance from the ponds, because there is no hot water in the surficial materials to a depth of at least 76 m (250 feet). The low permeability of the surficial materials east of the fault together with the northwestward sloping regional water table surface, prevent the warm water from moving eastward in the near surface. West of the fault, fractured quartzite and quartzite gravels beneath the surface act as a near surface reservoir in which water of approximately 86°C is stored. The reservoir of heated water warms the impermeable, confining, clay or low thermal conductivity by conduction. Together, the variable thickness of clay and the distribution of warm water produce the observed shallow ground temperatures to the west of the fault.

The spring orifices are found along zones of weakness in the clay that confines the near surface reservoir. The zones of weakness in the clay are coincident with the buried fractures described in previous sections of this report. Slight movement on the faults in question after the deposition of the confining clay, would cause the weakness in the clay to develop, and the water flows to the surface under the artesian conditions present in the near surface reservoir.

SUMMARY

The preceding report details research done over the past two years by UGMS at the Crystal Hot Springs system. Emphasis has been placed on reporting results of investigations, and the authors have consciously refrained from drawing definitive conclusions about many detailed aspects of the system. Research efforts either on going or planned (primarily geophysical surveys) may significantly alter the conception of structural geometry presented above. Further reports will be issued as results become available.

In summary, the Crystal Hot Spring geothermal system is a fault controlled convective system in which meteoric water circulates to depth and is warmed in the normal heat flow of the Basin and Range province. A significant portion of the preceding discussion focused on the location of faults in the vicinity of the spring system. The reason for this emphasis is the importance of faults in: a)

transporting deep thermal waters to the surface, and b) influencing the near surface expression of the resource. Without an understanding of the systems structural controls, development of the system will be hap-hazard and incomplete. Not all of the faults represented in this report transport thermal waters to the near surface. Therefore, the distribution of thermal waters in the near surface is also important. The use of shallow ground-temperature measurements, and gradient hole drilling have been used to obtain this information. By carefully interpreting the observed distribution of thermal water, the effects of very shallow ground-water systems can be eliminated and the source of the thermal water can be more clearly identified. The rate at which water will be produced from the system will only be determined by additional testing; the only available pump test was a test of a well completed in surficial sands. Similarly, the results of extensive use of the resource will only be determined after an extended period of production pumping.

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APPENDIX A

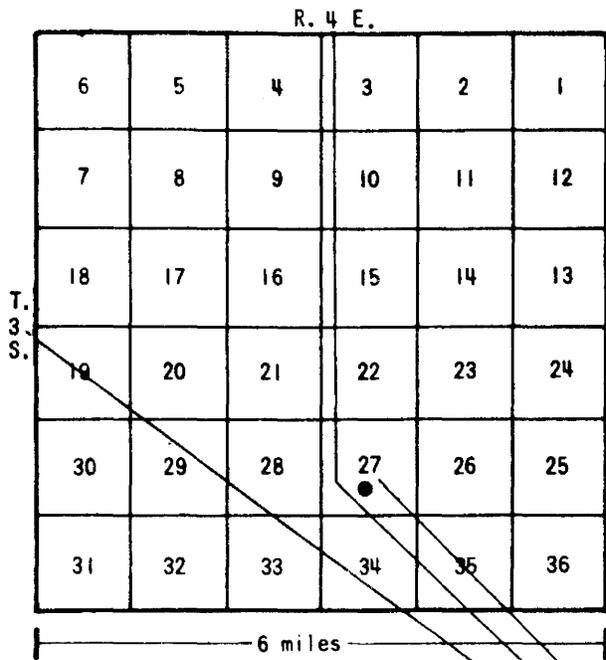
WELL - AND SPRING-NUMBERING SYSTEM

THERMAL GRADIENT HOLE LITHOLOGIC LOGS

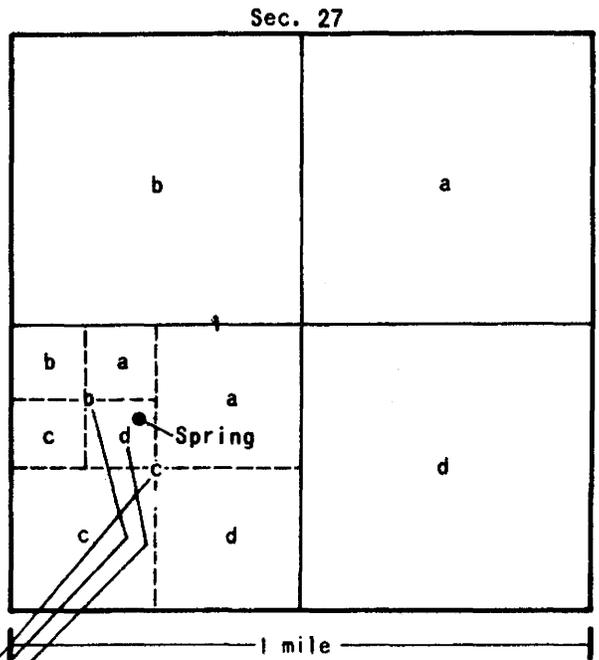
ABBREVIATIONS

MT = MUD TEMPERATURE

Sections within a township



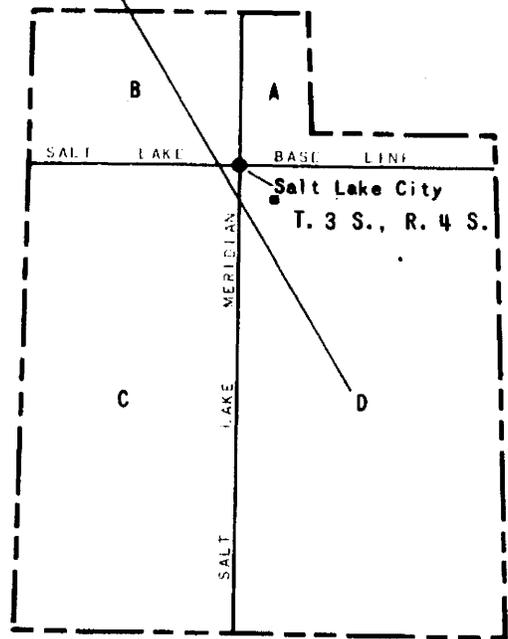
Tracts within a section



(D-3-4)27cbd-S1

Spring-numbering System

The spring-numbering system used in this report is shown in figure 1 and is based on the U. S. Bureau of Land Management's system of land subdivision. The spring number indicates the location of the spring by quadrant, township, range, section, and position (if known) within the section. Four quadrants are formed by the intersection of the Salt Lake Base Line and the Salt Lake Meridian. The capital letter at the beginning of the location code indicates the quadrant in which the spring is located—A the northeast quadrant, B the northwest, C the southwest and D the southeast. Numbers designating the township and range, respectively, follow the quadrant letter, and the three are enclosed in parentheses. The number after the parentheses designates the section; the lowercase letters, if shown, indicate the location of the spring within the section. The first letter denotes the quarter section (usually 160 acres), the second the quarter-quarter section (40 acres), and the third the quarter-quarter-quarter section (10 acres). The letters are assigned within the section in a counterclockwise direction beginning with "a" in the northeast quarter of the section. Letters are assigned within each quarter section and each quarter-quarter section in the same manner. The capital letter "S" completes the designation of a spring. When two or more springs are within the smallest subdivision, consecutive numbers beginning with 1 are added after the letter "S." For example, (D-3-4)27cbd-S1 indi-



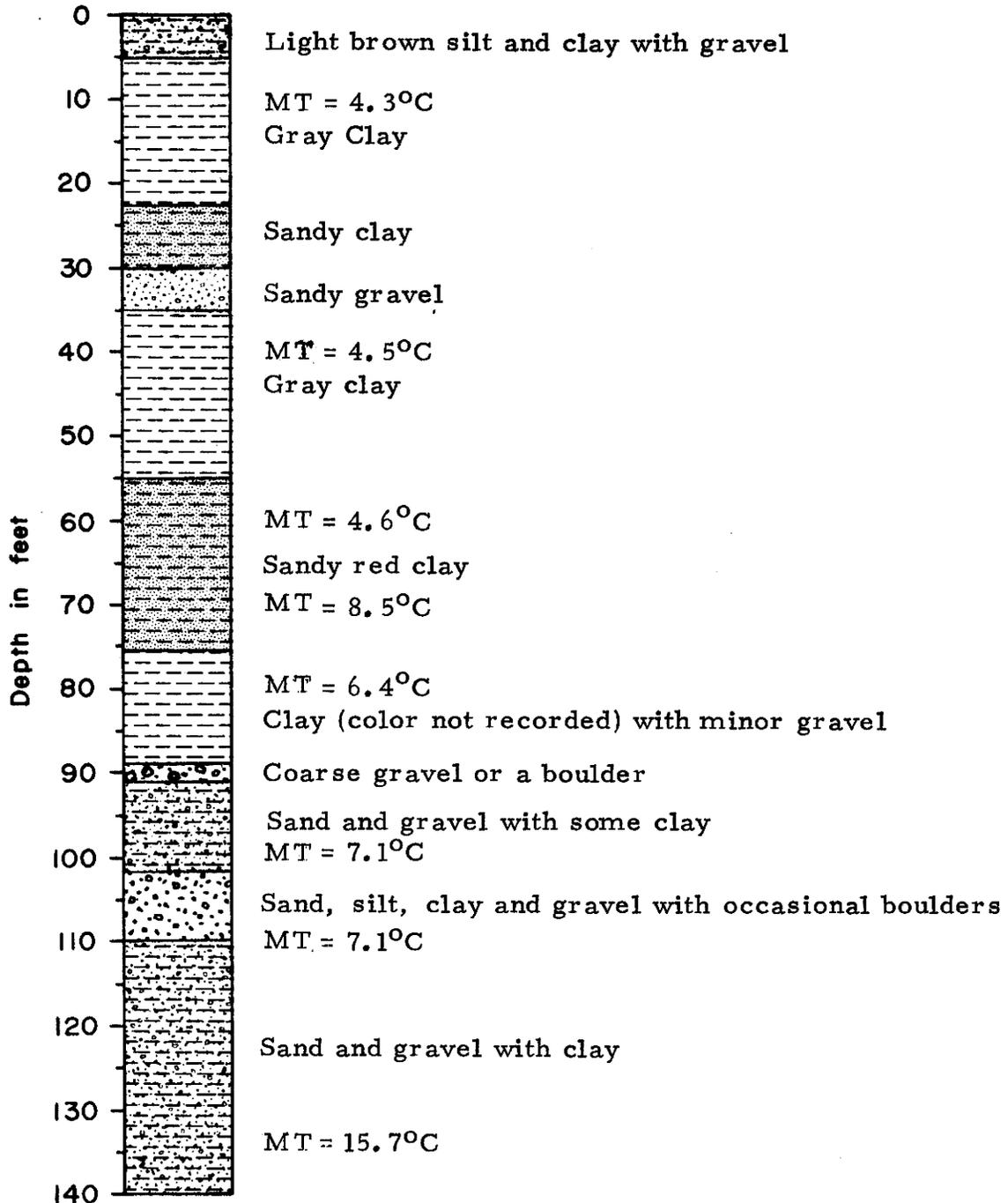
icates a spring in the southeast of the northwest quarter of the southwest quarter of sec. 27, T. 3 S., R. 4 E., and shows that this is the first spring recorded in the quarter-quarter-quarter section. The capital letter D indicates that the township is south of the Salt Lake Base Line and that the range is east of the Salt Lake Meridian.

Temperature Gradient Hole Log

Hole C/GH - A Location (C - 4 - 1) 12 bbd 1

Surface Elevation 4457' Comp. Date 2 - 20 - 78 T. D. 220'

Comments

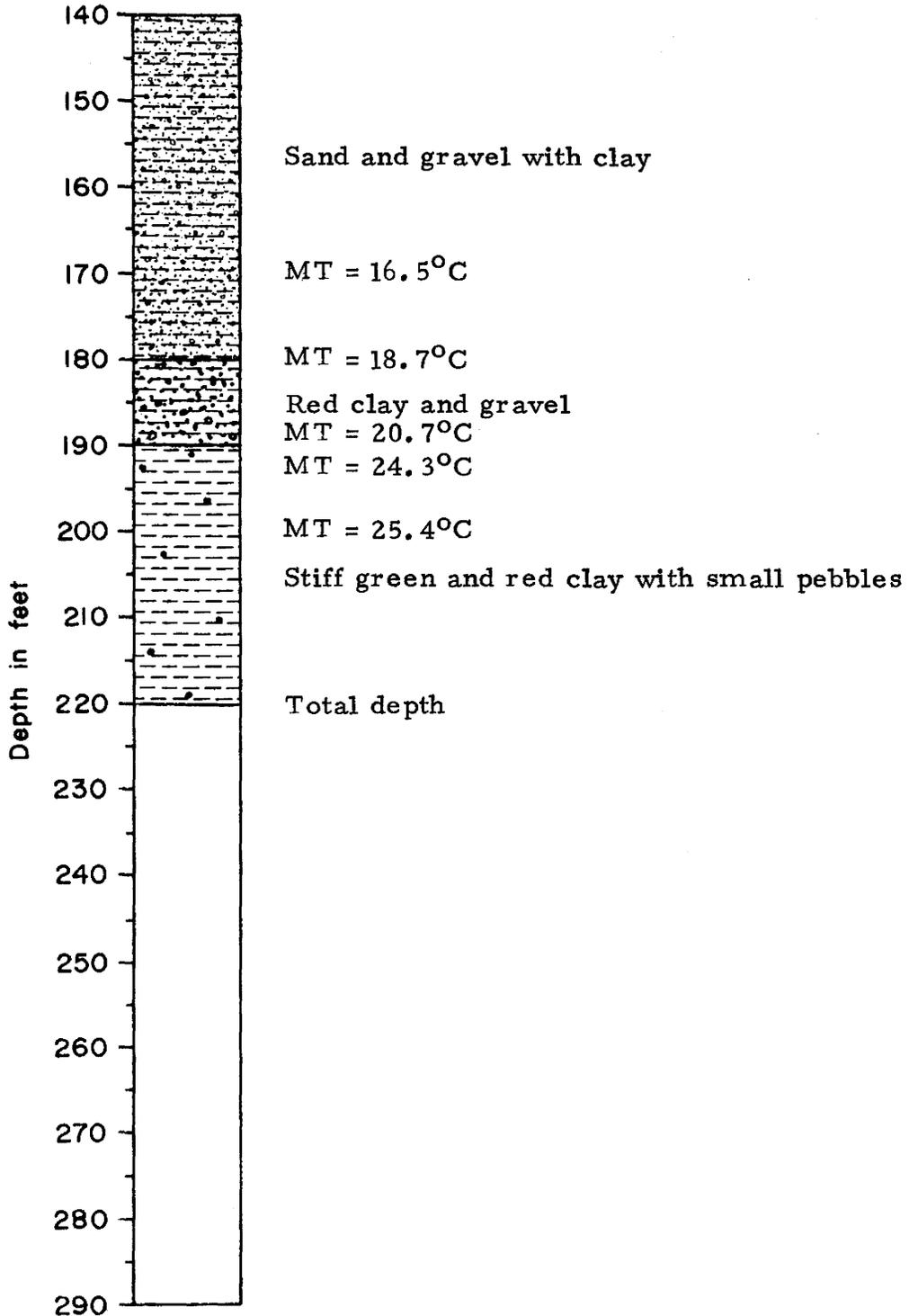


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - A (continued)

Comments

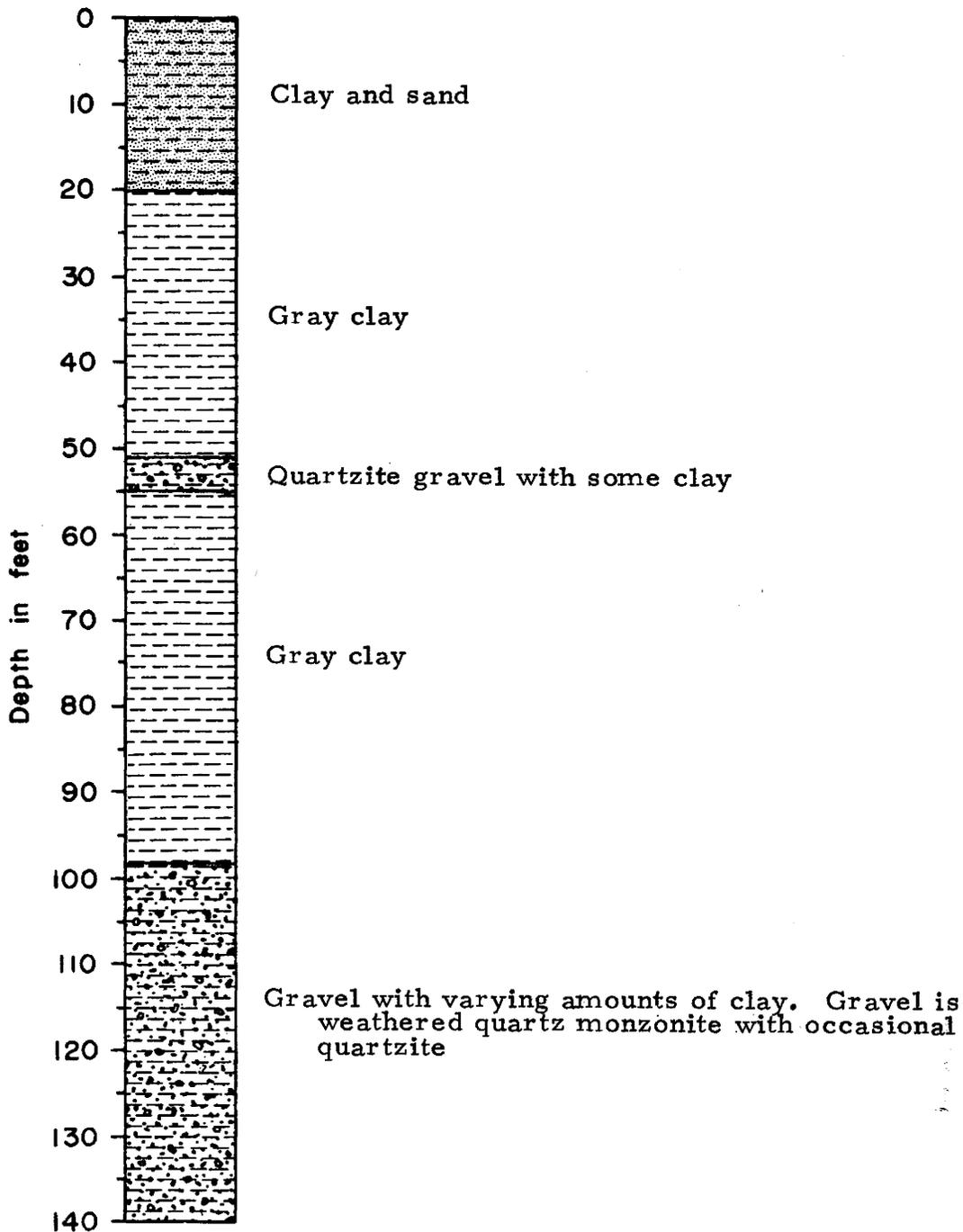


Temperature Gradient Hole Log

Hole C/GH - B Location (C - 4 - 1) 12 bac

Surface Elevation 4450' Comp. Date 2 - 23 - 78 T. D. 245'

Comments

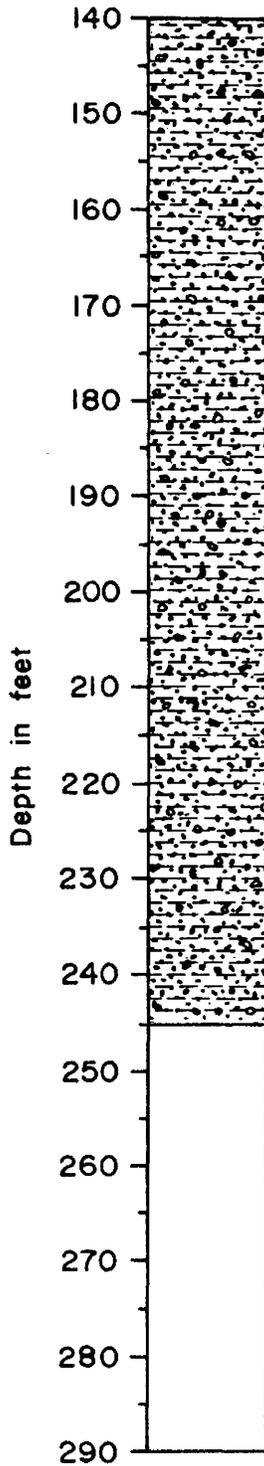


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - B (continued)

Comments



Gravel with varying amounts of clay. Gravel is weathered quartz monzonite with occasional quartzite

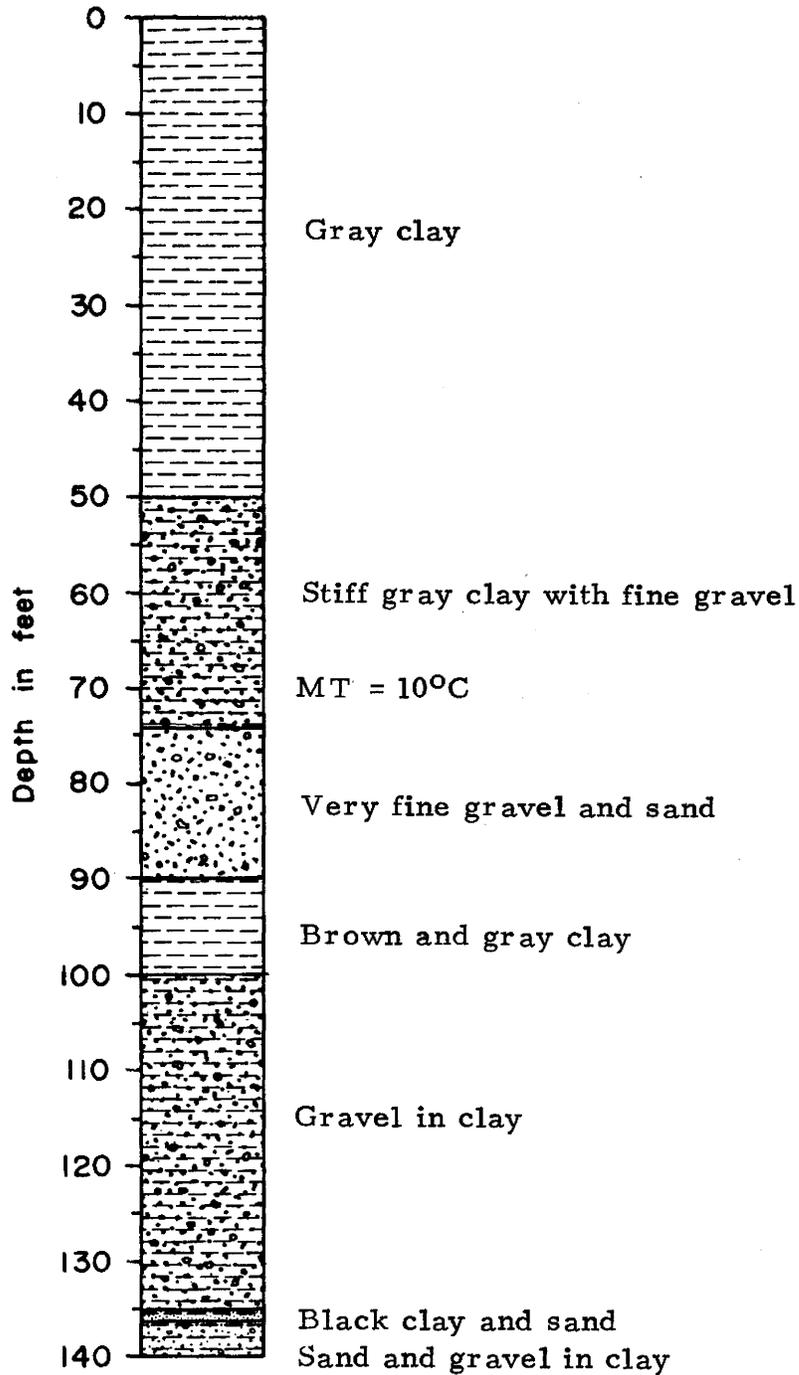
Total depth

Temperature Gradient Hole Log

Hole C/GH - C Location (C - 4 - 1) 11 add

Surface Elevation 4452' Comp. Date 2 - 24 - 78 T. D. 280'

Comments

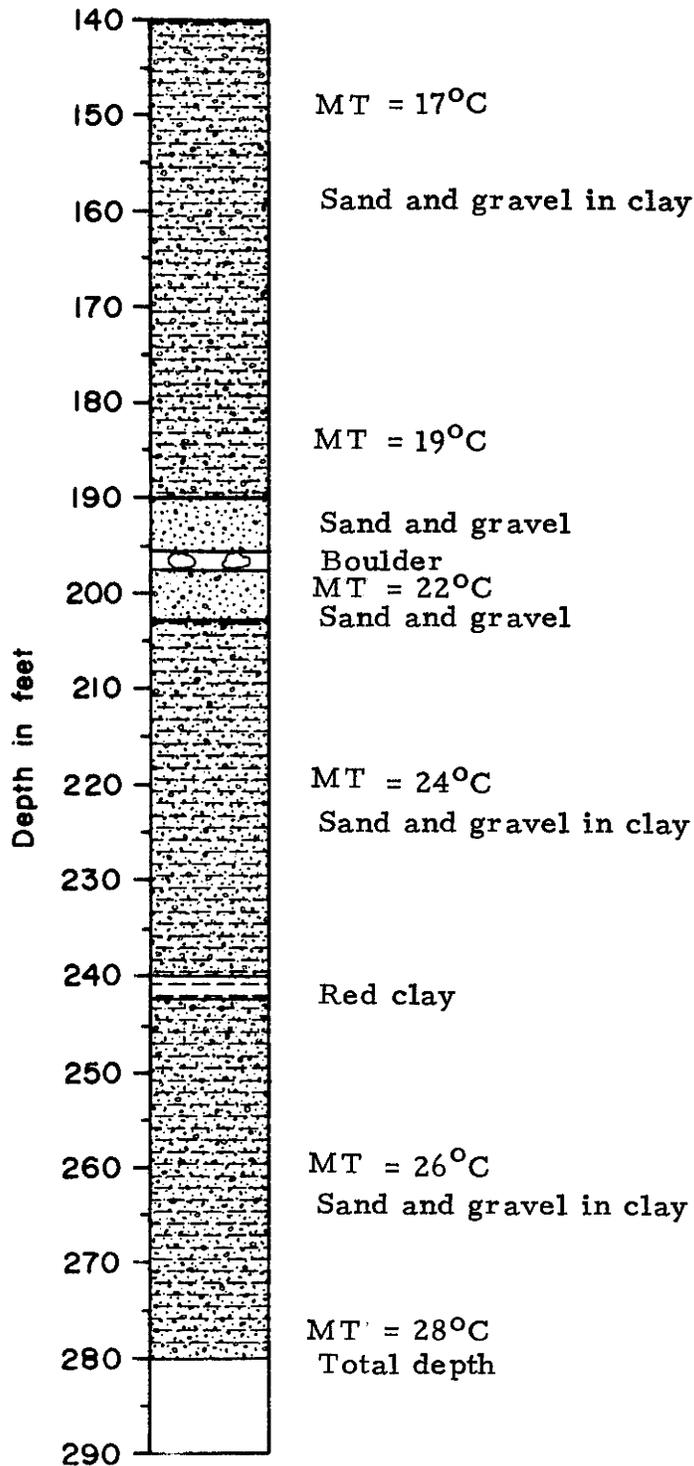


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - C (continued)

Comments

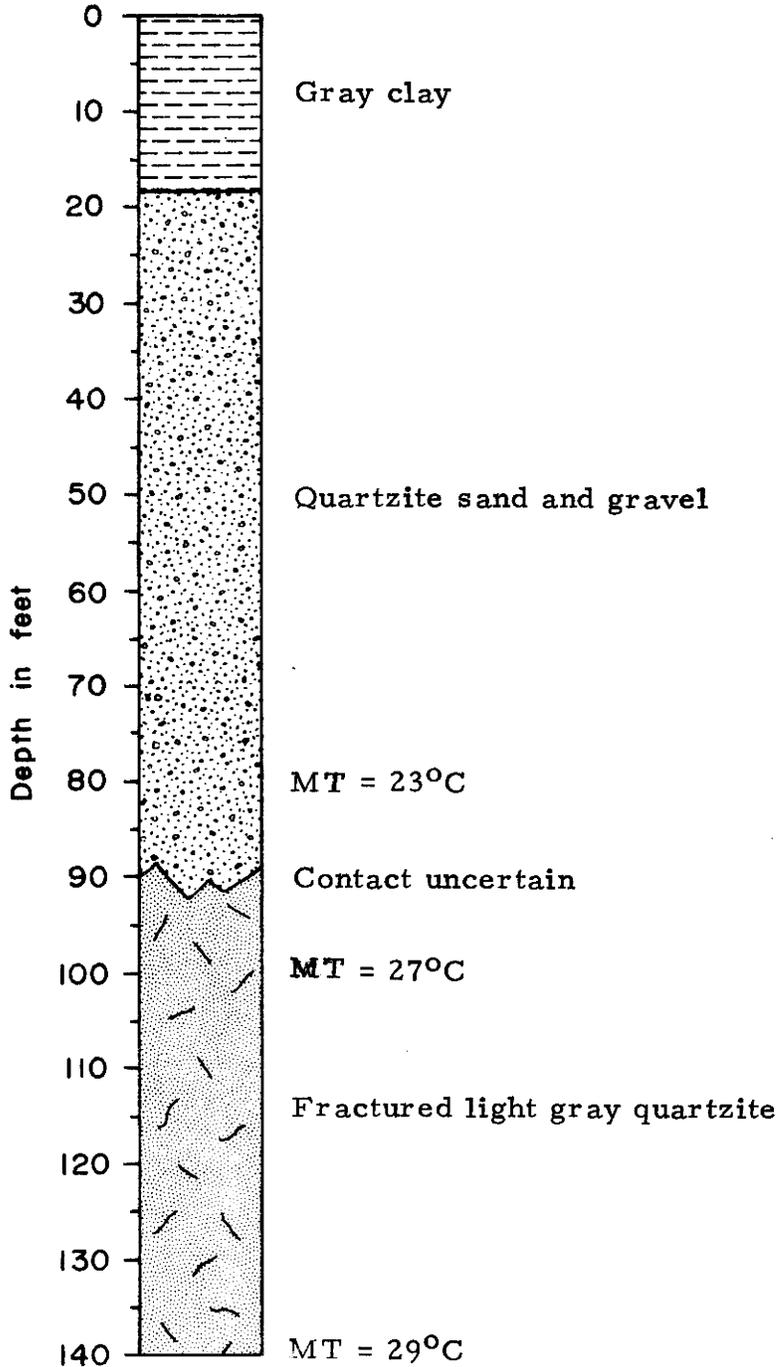


Temperature Gradient Hole Log

Hole C/GH - D Location (C - 4 - 1) 12 bcd

Surface Elevation 4472' Comp. Date 3 - 1 - 78 T.D. 237'

Comments

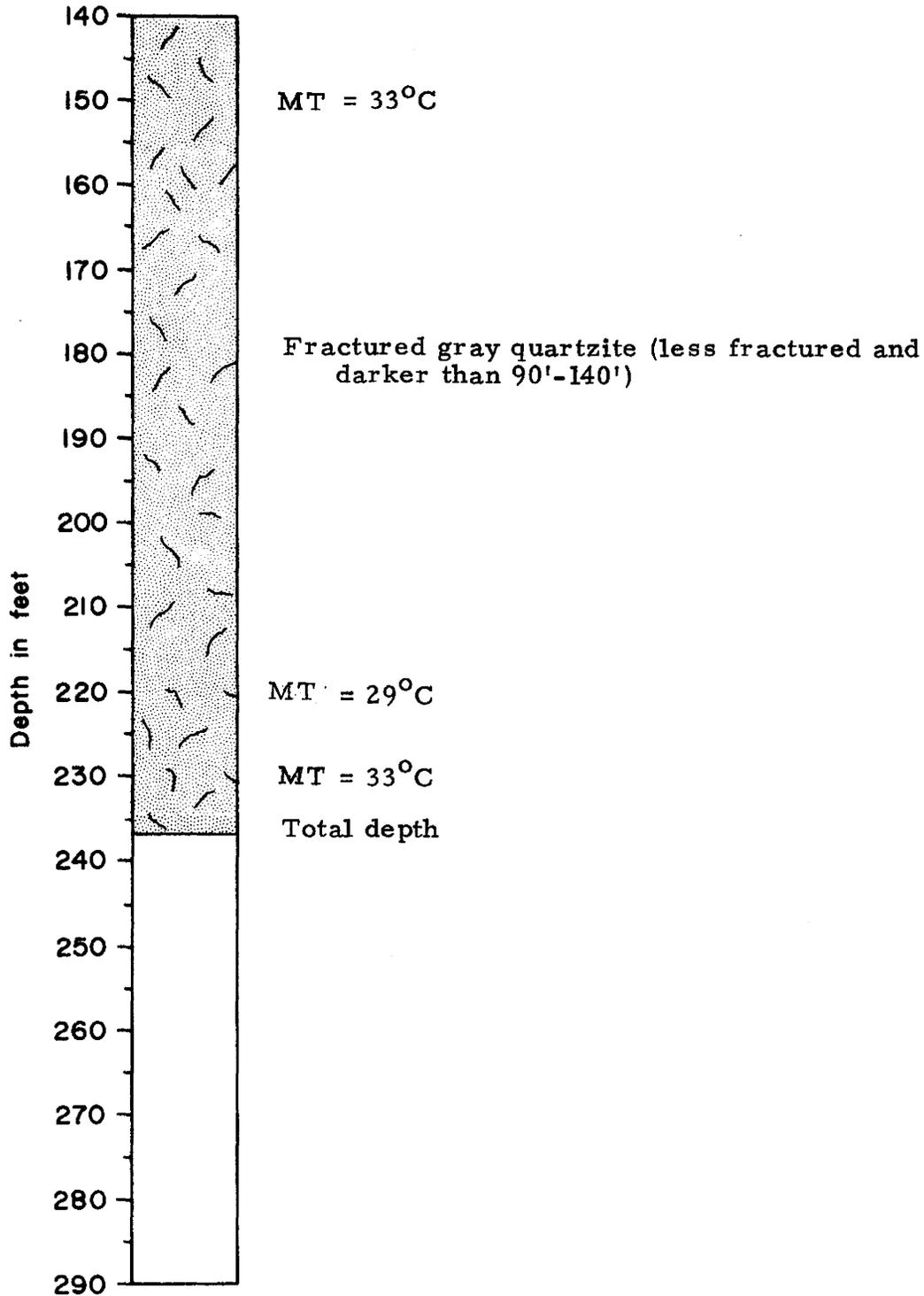


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - D (continued)

Comments

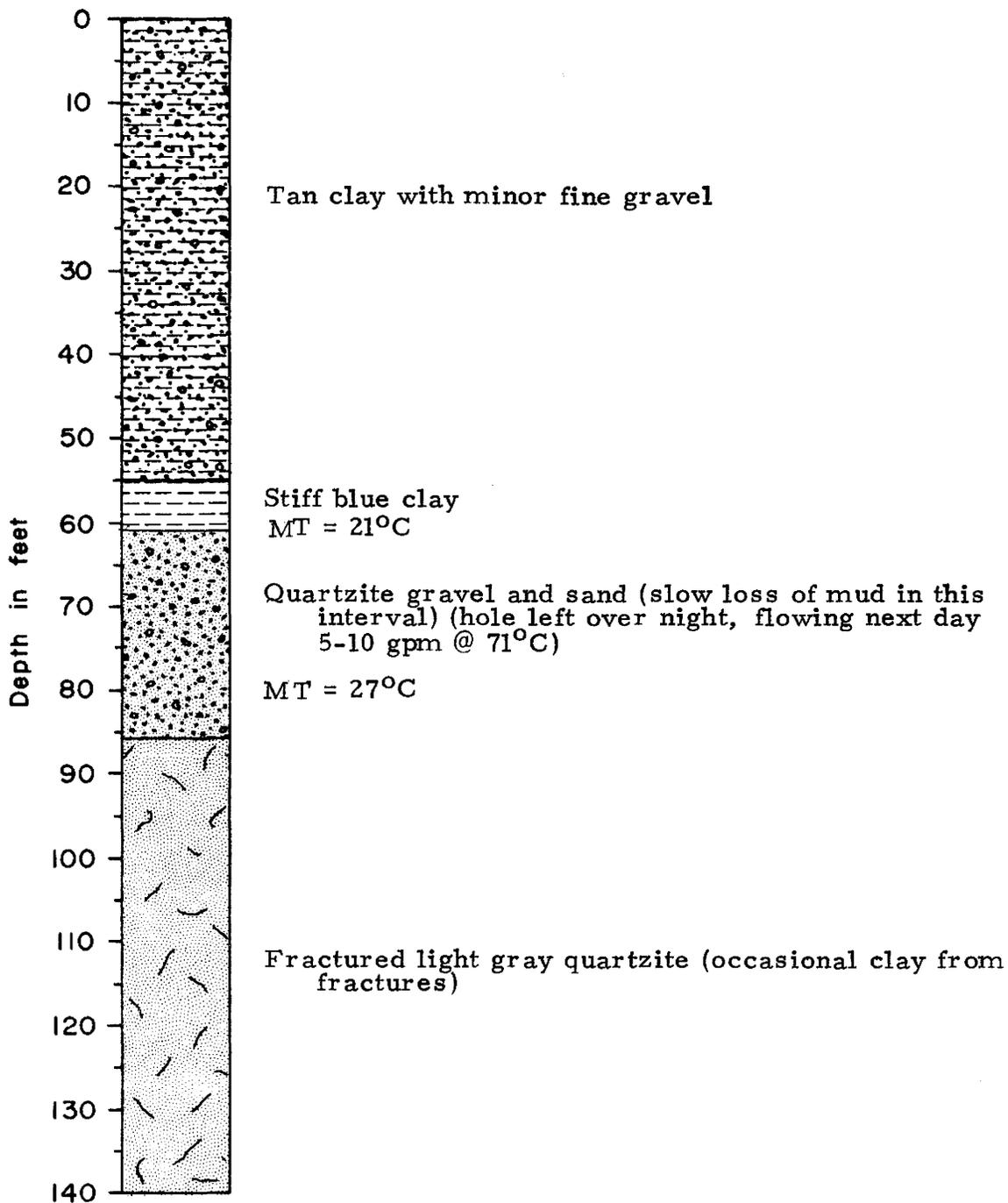


Temperature Gradient Hole Log

Hole C/GH - E Location (C - 4 - 1) 12 bbc

Surface Elevation 4465' Comp. Date 3 - 17 - 78 T. D. 200'

Comments

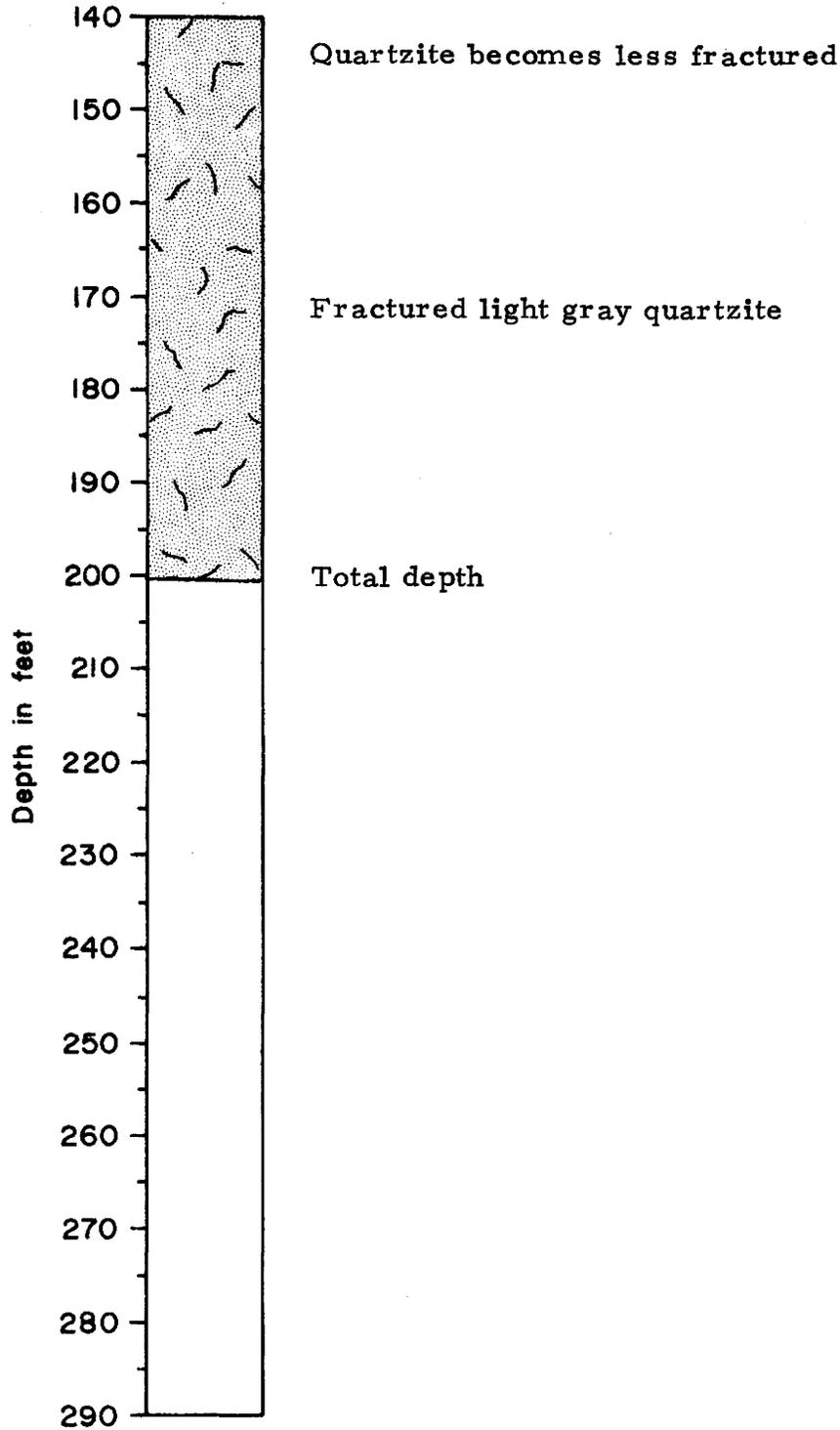


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - E (continued)

Comments

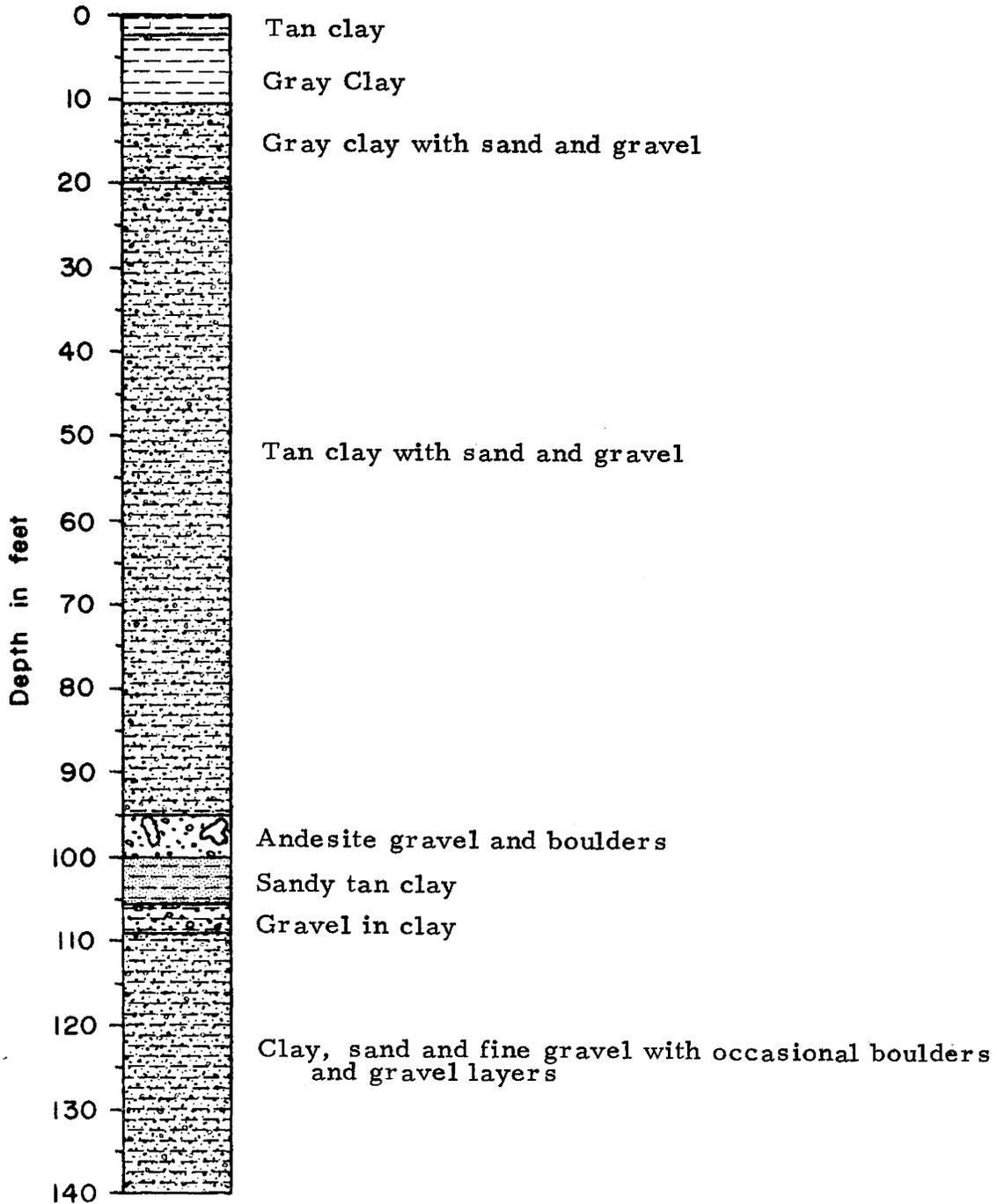


Temperature Gradient Hole Log

Hole C/GH - F Location (C - 4 - 1) 12 bdc

Surface Elevation 4483' Comp. Date - 21 - 78 T. D. 250'

Comments

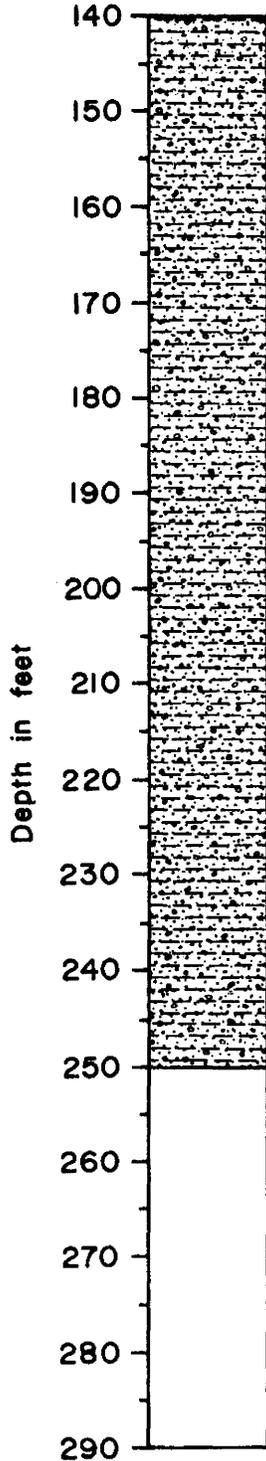


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/GH - F (continued)

Comments



Clay, sand and fine gravel with occasional boulders and gravel layers

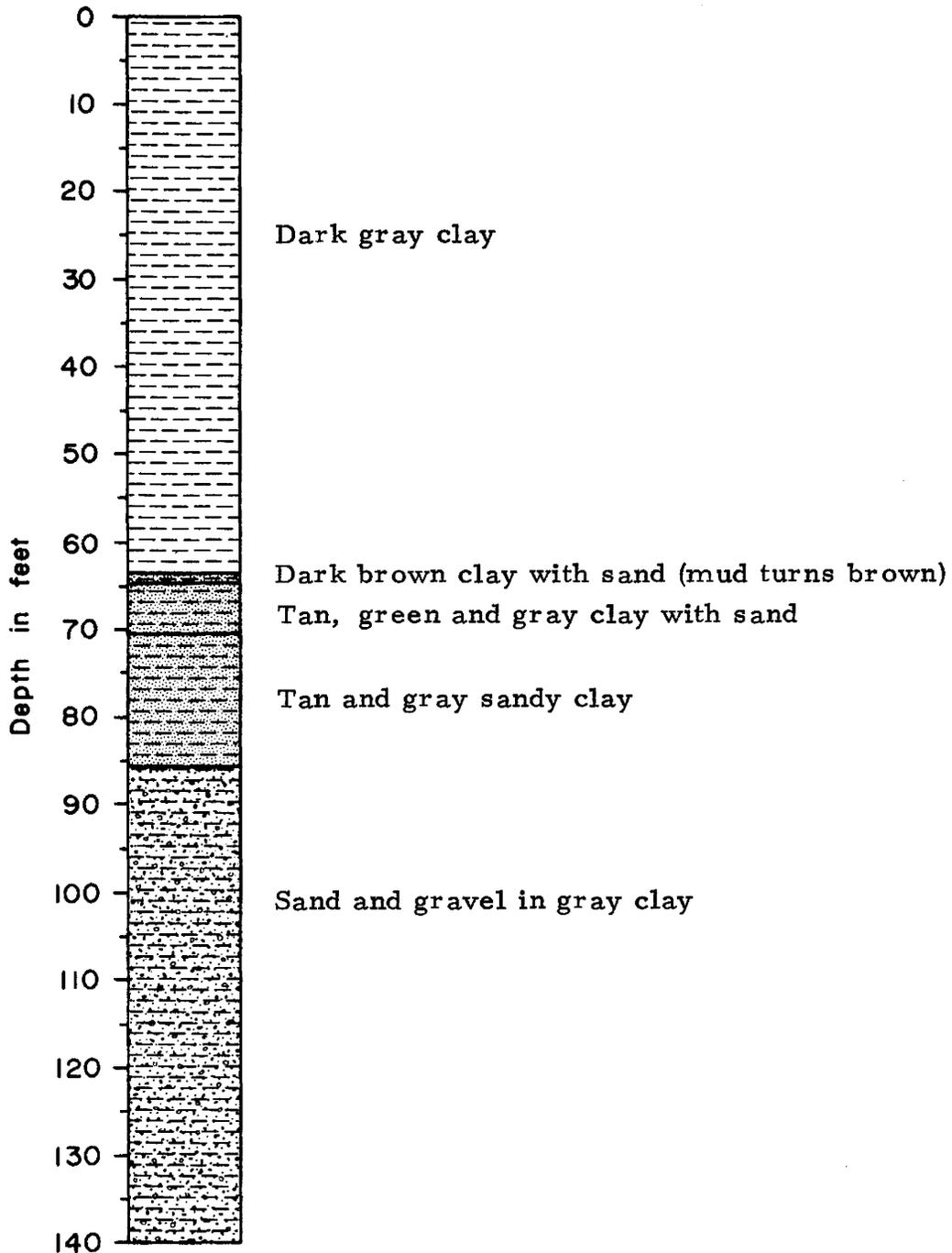
Total depth

Temperature Gradient Hole Log

Hole C/WW - SF Location (C - 4 - 1) 12 bbd 2

Surface Elevation 4460' Comp. Date 4 - 12 - 78 T. D. 280'

Comments

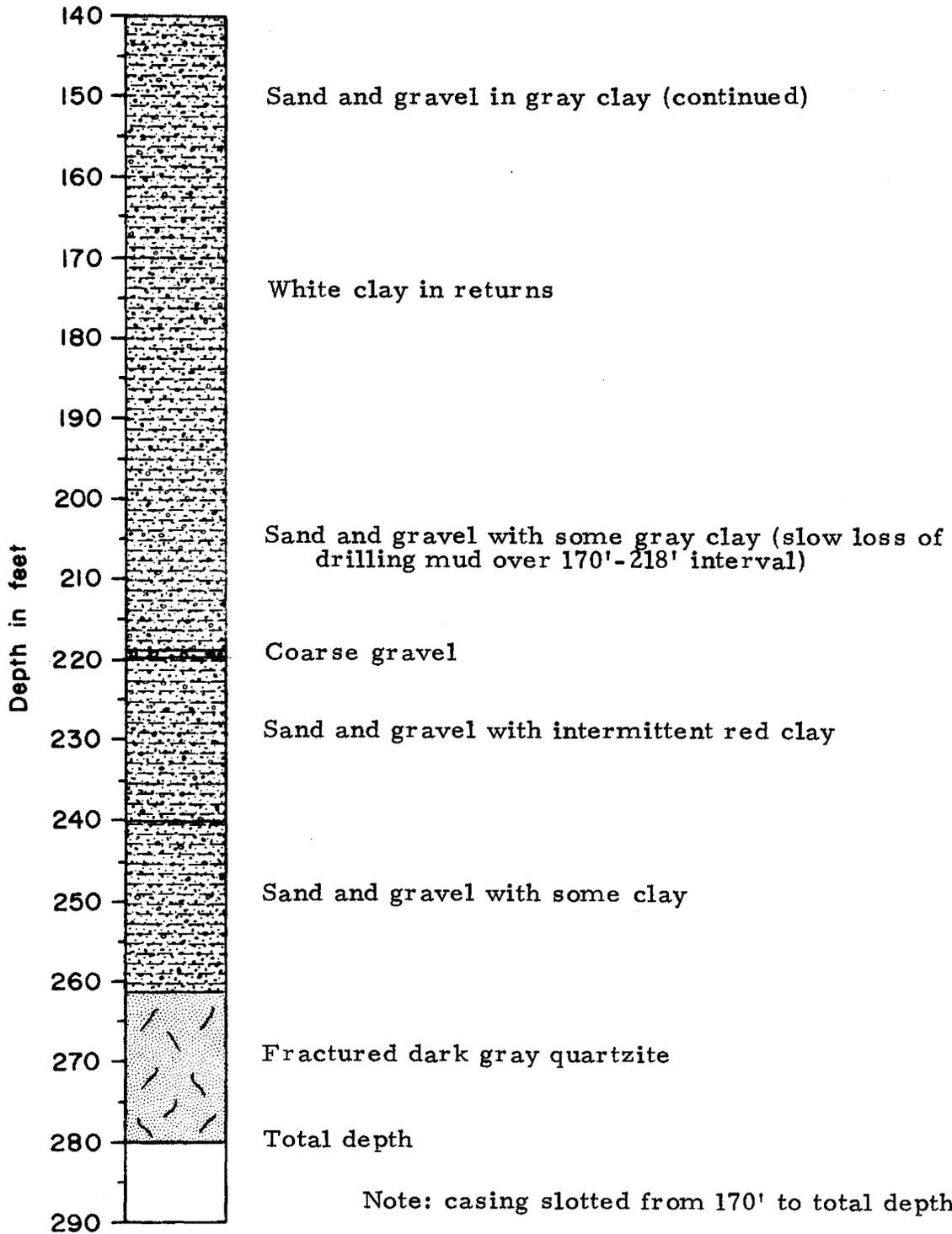


10 feet = 3.048 meters

Temperature Gradient Hole Log

Hole C/WW - SF (continued)

Comments



Note: casing slotted from 170' to total depth.

Name: Lee
 Owner: Utah State Board of Corrections
 Location: (C-4-1)2ddb
 Driller's Log:
 0-3 top soil
 3-82 blue clay
 82-119 hard pan and sand
 119-200 conglomerate
 200-205 gray clay
 205-248 conglomerate and gravel
 248-309 conglomerate
 309-340 gravel and a little water
 340-397 sand and gravel
 397-427 sand and gravel
 427-463 gravel and clay
 463-503 gumbo clay
 503-552 sticky clay
 552-582 sand and clay
 582-603 sticky clay
 603-665 gravel and clay
 665-707 sticky clay
 707-722 clay and gravel
 722-825 bedrock

Name: None
 Owner: Evan W. Hanson
 Location: (C-4-1)13ccc
 Driller's Log:
 0-3 silt
 3-99 silt, sand, and gravel
 99-148 conglomerate
 148-195 clay sand and gravel
 195-226 sandy clay
 226-236 gravel with water
 236-241 sand and gravel
 241-249 fractured quartzite and water
 250-290 solid rock

Name: None
 Owner: Karl Dean
 Location: (C-4-1)11acc
 Driller's Log:
 0-45 brown clay
 45-90 blue clay
 90-110 sand
 110-150 sand and gravel

Name: None
 Owner: Loran D. Dixon
 Location: (C-4-1)13bab
 Driller's Log:
 0-3 silt and sand
 3-9 gravel
 9-11 clay
 11-30 gravel
 30-38 cobbles
 38-109 fractured quartzite
 109-117 gravel and water
 117-121 solid rock
 121-140 open hole

57-7922
016486

Name: Hall
 Owner: Donald W. Hall
 Location: (C-4-1)11dad
 Driller's Log:
 0-76 clay (top soil)
 76-127 sandy clay
 127-138 sand and gravel (heaved in hole)
 138-140 coarse gravel
 140-157 clay and gravel
 157-174 brown sandy clay
 174-182 white rock
 182-196 blue shale
 196-215 clay and gravel
 215-236 gray sandstone
 236-262 black sandstone
 262-271 bedrock - hard gray
 271-290 clay and sand

Name: None
 Owner: Mount Jordan Corporation
 Location: (C-4-1)14dcd
 Driller's Log: (hole deepened)
 438-455 conglomerate
 455-466 sand and gravel
 466-472 conglomerate
 472-490 clay and gravel
 490-520 gravel
 520-550 clay and gravel
 550-555 gravel
 555-590 clay and gravel
 590-715 clay
 715-716 gravel
 716-718 clay and gravel
 718-758 clay
 758-761 sand and clay
 761-815 clay
 815-821 sand and gravel
 821-845 clay

Name: None
Owner: Kenneth White
Location: (C-4-1)23aaa
Driller's Log:
0-3 topsoil
3-165 dry sand and gravel
165-180 clay and gravel
180-200 dry sand and gravel
200-365 clay and gravel
365-375 conglomerate
375-523 clay and gravel

Name: None
Owner: Gene Whendon
Location: (D-4-1)6caa
Driller's Log:
0-5 top soil
5-25 bentonite clay
25-27 gravel with water
27-65 clay (bentonite) and sand
65-75 quick sand
75-105 sand and bentonite
105-117 sand and gravel and bentonite
117-125 sand and gravel
125-133 bentonite (sealed off water)
133-143 sand, gravel and bentonite
143-165 sand and gravel with little bentonite
165-170 cobbles
170-178 sand and gravel (bentonite)
178-180 quick sand
180-210 sand, gravel, and little bentonite.

Name: None
Owner: Boyd A. Fitzgerald
Location: (D-4-1)7bbb
Driller's Log:
0-5 top soil
5-92 clay and gravel
92-94 sand and gravel with water
94-123 clay and gravel
123-125 gravel with water
125-139 clay and gravel
139-167 gravel with water

APPENDIX B

PUMP TEST DATA

AND ANALYSES OF

C/WW - SF

Pump Test Data from C/WW - SF 11/7/78

<u>Time of Day</u>	<u>Water Level</u>	<u>Discharge</u>	<u>Notes</u>
2:32	Above Ground	50 gpm	Engine RPM's set to 1500
2:35	35		
2:37		35 gpm	
2:38	38		
2:40	39		
2:42	43		
2:44	45	25 gpm	
2:47	47	26 gpm	
2:50	47		
2:52	48	28 gpm	
2:56	48		
3:00	47	30 gpm	
3:03	46		
3:09	46	28 gpm	
3:14	46	29	
3:36	47	30	
3:46	47	30	
3:56	48	30	
4:11	48	27	
4:27	43	28	Engine changes RPM's
4:41	48	28	
5:05	47	30	
5:22	48	30	
5:33	43	30	Engine changes RPM's Engine RPM's increased to 1700
5:35	69	37	
5:40	78	32	
5:43	78		
5:51	81	30	
6:00	82	29	
6:15	84	30	
6:32	84	30	
6:46	84	30	
7:00	84	27	
7:17	84	30	Engine RPM's increased to 2000
7:20	123	40	
7:23	123	38	
7:28	125	38	
7:36	126	38	
7:45	126	38	

Pump Test Data from C/WW - SF 11/7/78 (continued)

<u>Time of Day</u>	<u>Water Level</u>	<u>Discharge</u>	<u>Notes</u>
8:00	127	35	
8:15	127	35	
8:30	128	38	
8:46	127	38	
8:49	127	38	
8:50	Recovery		Pump turned off
15 secs.	85		
20	75		
32	72		
40	68		
45	66		
60	63		
65	60		
70	57		
80	54		
90	51		
100	48		
110	45		
120	43		
125	41		I seriously question
132	39		anything above 40 ft.
140	37		draw down and would
160	35		not use.
190	33		
210	Flowing at surface		

PETER J. MURPHY
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UURI

EARTH SCIENCE LABORATORY
391 CHIPETA WAY, SUITE A
SALT LAKE CITY, UTAH 84108
801-581-5283

December 15, 1978

Pete Murphy
UGMS
606 Blackhawk Way
Salt Lake City, UT 84108

Dear Pete:

The results of the November 7, 1978 pump test of the flowing geothermal well near Crystal Hot Springs are encouraging. The aquifer can probably support several more low-capacity wells without diminishing the natural discharge to the ponds at Crystal Hot Springs.

The alluvial aquifer is tight, and large diameter wells may not be able to produce more water than smaller, less costly wells. All wells should be completed in bedrock.

I believe that the fractured quartzite is leaking hot water to the overlying alluvial aquifer. An observation well and an additional pump test will be needed to assess this inferred leakage and the accompanying vertical movement of water and delayed yield from storage.

A thin hole within 30 feet of the flowing well, similar to the temperature gradient holes but with perforated PVC casing, would be an adequate observation well that might later be adaptable to production.

Sincerely,



Christian Smith

CS/smk

encl.

cc: P.M. Wright
D. Foley

CRYSTAL HOT SPRINGS PUMP TEST ANALYSIS

The flowing geothermal well on the grounds of the Utah State Prison near Crystal Hot Springs, Jordan Narrows Quadrangle, Utah was pumped at an average rate of 30 gpm for more than six hours on November 7, 1978. This report summarizes the data and results of this short-term pump test.

Figure 1 is a sketch of the well and the geologic units it penetrates. The well diameter is 6 in, its total depth 285 ft; it is cased to the bottom of the hole. Torch-cut slots in the bottom 110 ft of the casing were used to complete the well. The artesian head is inferred to be 9 ft above ground level; artesian flow is about 8 gpm at 180°F. The 195 ft thick, fine-grained alluvial aquifer is confined above by approximately 90 ft of clay and below by quartzite bedrock. The quartzite is pervasively fractured and locally supplies hot water to the overlying aquifer. While it is not known whether the quartzite yields water directly to the well, it is certain that it does leak hot water to Crystal Hot Springs, a few hundred feet to the south.

The pump test was designed to be, but did not satisfy the strict requirements for, a step-drawdown test and its numerical analysis. Attempts to apply the step-drawdown analysis suggest well-losses are minimal and that the well is efficient. Completion of the well may even have improved the transmissivity of the aquifer within a short distance of the well.

The raw pump test data are plotted in Figure 2. Discharge, Q , in gallons per minute and drawdown (the increasing depth to water), s , in feet are plotted against the logarithm of time. A nearly constant rate of discharge at 30 gpm was sustained for 288 minutes. During this interval the drawdown was also nearly constant (at 57 and 93 feet). Drawdown increased only when

discharge exceeded 30 gpm (between 0 and 12 min., and 183 and 188 min.). These observations indicate that there is a source of hot water near the well capable of supplying about 30 gpm instantaneously to the aquifer. The constant drawdown (136 ft) during the final pumping interval indicates that the source of hot water may be capable of supplying as much as 35 gpm.

The source of hot water also fills the ponds at Crystal Hot Springs. It is possible but unlikely that the well is pumping water that would otherwise rise to these ponds. It is also possible that the quartzite is leaking water directly to the well. In either case, pumping 30 gpm should have no observable effect upon the natural regime of the ponds.

Since no observation wells were available, the log-log type curve solution for transmissivity, T , and storage, S , cannot be found. To estimate T , the 'Harrill time', t_H , was used in a conventional straight-line analysis of the recovery data (Fig. 3). This value compensates for the changes in discharge and the nonequal periods of pumping at the different discharges recorded during the test (Harrill, 1970). Two straight-line segments emerged, an 'early' segment and a 'late' segment, from which the corresponding transmissivities T_e and T_l can be computed.

$$T_e = 34.4 \text{ ft}^2/\text{day}$$

$$T_l = 18.7 \text{ ft}^2/\text{day}$$

These values are low but are typical of tight, fine-grained artesian aquifers.

The two estimates of T are sufficiently low to limit the rate at which the aquifer can deliver water to the well. When pumped at a rate less than it can deliver, an aquifer with a low T and a nearby source of water is likely to

sustain a constant drawdown. The response in an artesian system may be instantaneous: an increased discharge can cause the water level to drop immediately. If the pumping rate is again dropped to the lower rate, the water level will again remain constant, but at a lower level. This is thought to be what happened during the pump test at Crystal Hot Springs.

Given an estimate of T and the pump-test data, it is possible to estimate the value of storage, S . The well was pumped for 0.26 days at an average discharge of 30 gpm; the total drawdown was 135 ft. The solutions are not strictly valid for reasons discussed below but they are

$$\begin{array}{ll} T_e = 34.4 \text{ ft}^2/\text{day} & S = 0.001 \\ T_1 = 18.7 \text{ ft}^2/\text{day} & S = 0.05 \end{array}$$

Figure 4 is a graph of drawdown as a function of the logarithm of distance from the pumping well for these two solutions. Tables 1 and 2 are the values plotted in Figure 4. Data from an observation well within 30 ft of the pumping well would discriminate between these two solutions. Both values of S are high for artesian systems; the value of $S = 0.05$ is so high that the T_1 solution is less likely.

The Theis equation has been used to predict the effects of continued pumping on the aquifer (Theis, 1935), and it assumes an infinite isotropic aquifer with no recharge areas near the pumping well, conditions violated at Crystal Hot Springs. Since a recharge area is indicated at Crystal Hot Springs, the Theis equation predicts drawdowns greater than those that will probably be observed. The drawdowns listed in Tables 3a-d and 4a-d and shown in Figures 5 and 6 may be excessive and the values of S too great.

Figures 5 and 6 plot the drawdown as a function of the logarithm of distance from a well pumping 10 gpm for periods of one day, one month, one year, and ten years. It can be seen that continued pumping of the present well is predicted to have little effect on the Crystal Hot Springs area. The aquifer may be able to support several properly spaced small-diameter wells pumping 10 gpm in a well field.

Before production is contemplated, an observation well should be drilled near the present well and a flow test run. The leaky confined aquifer equation of Hantush (1959) could then be used to refine the conclusions presented here.

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- Theis, C. V., 1935, The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using ground-water storage: Amer. Geophys. Union Trans. pt. 2, p. 517-524

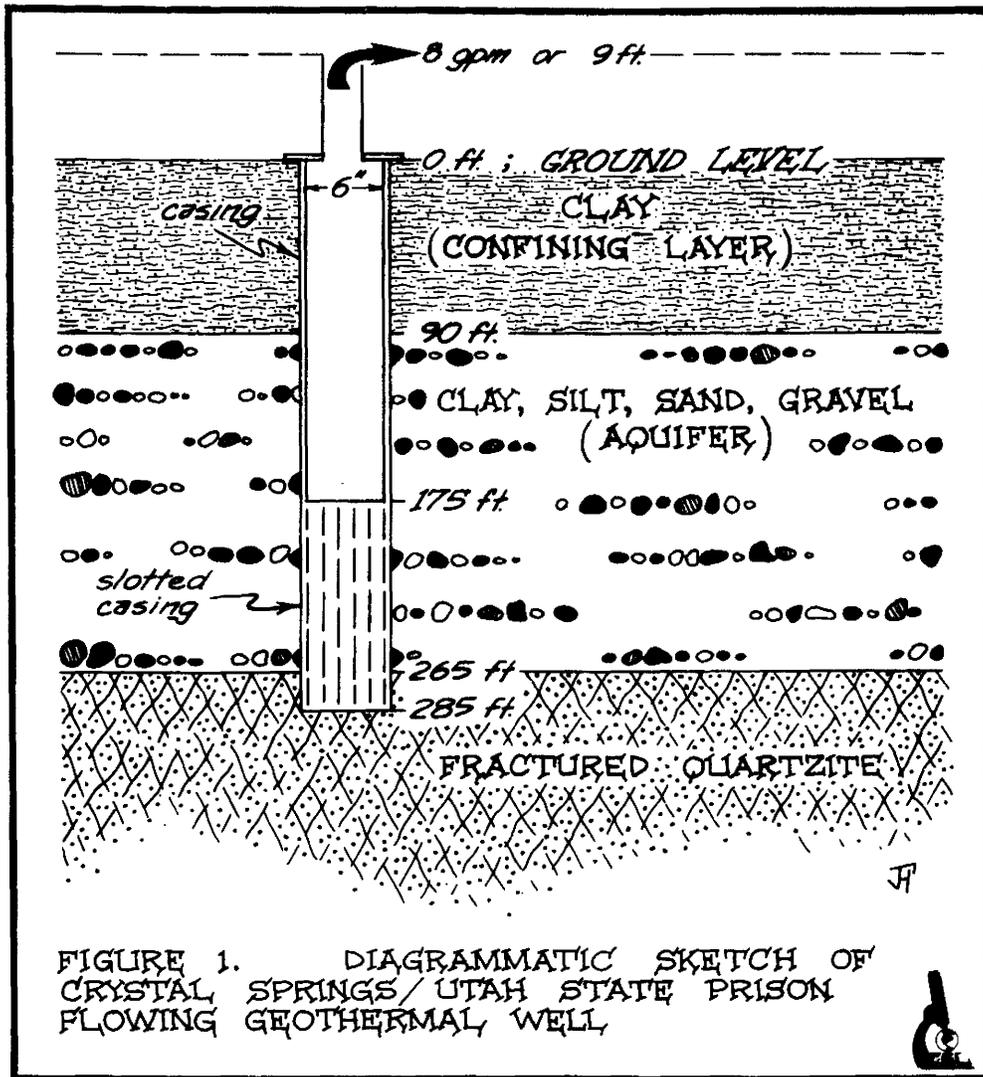


FIGURE 1. DIAGRAMMATIC SKETCH OF CRYSTAL SPRINGS/UTAH STATE PRISON FLOWING GEOTHERMAL WELL



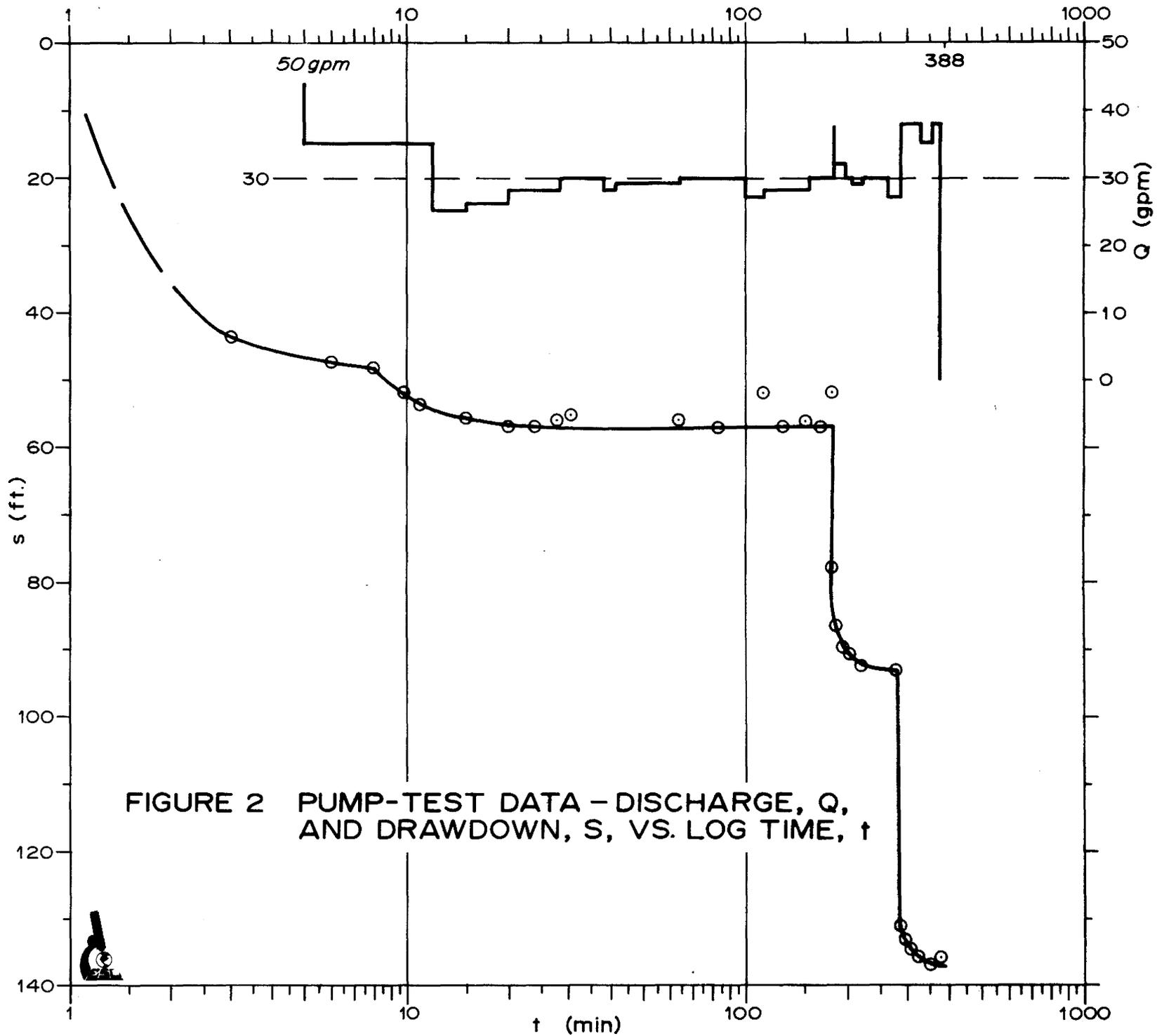
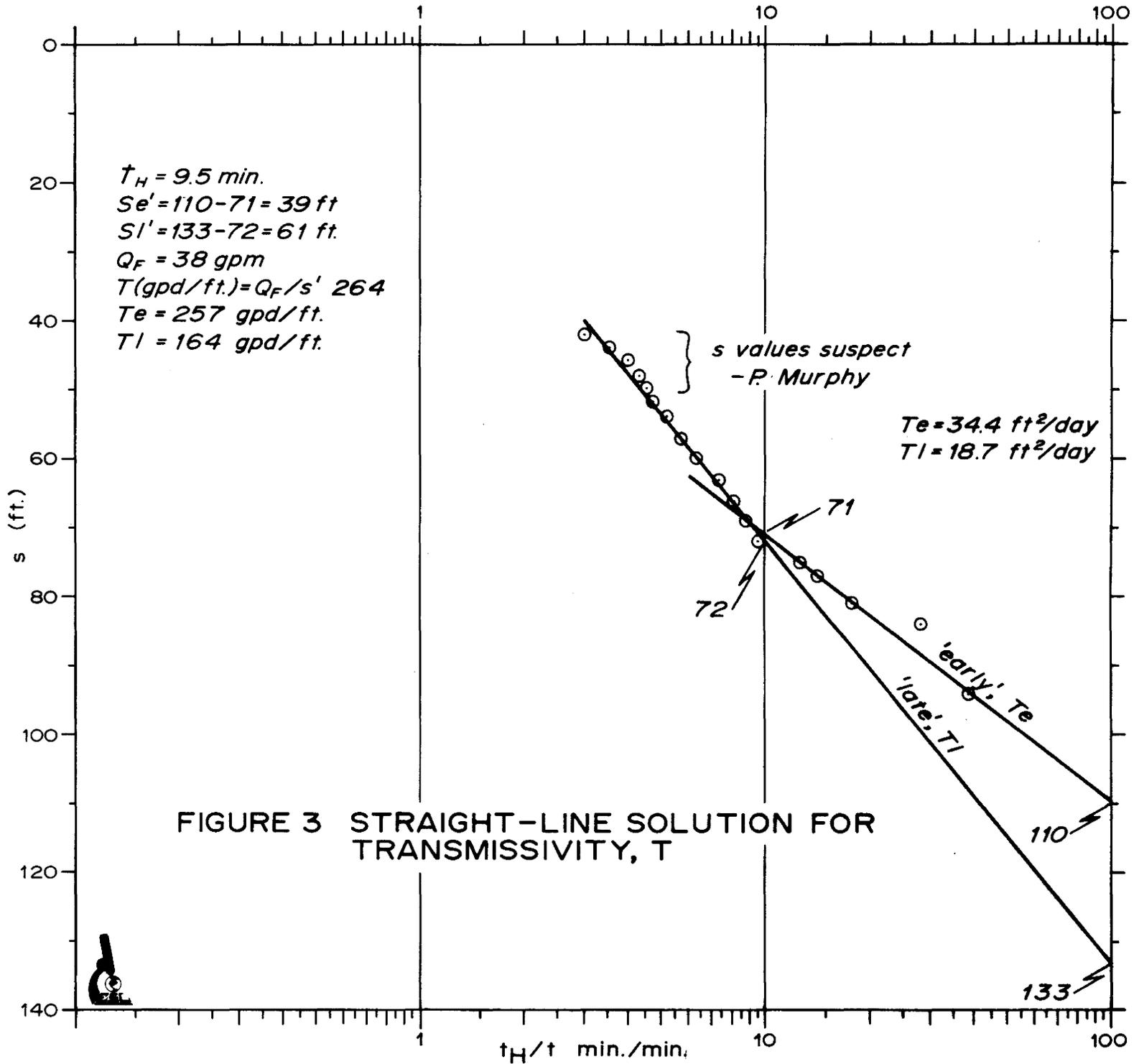


FIGURE 2 PUMP-TEST DATA - DISCHARGE, Q , AND DRAWDOWN, S , VS. LOG TIME, t



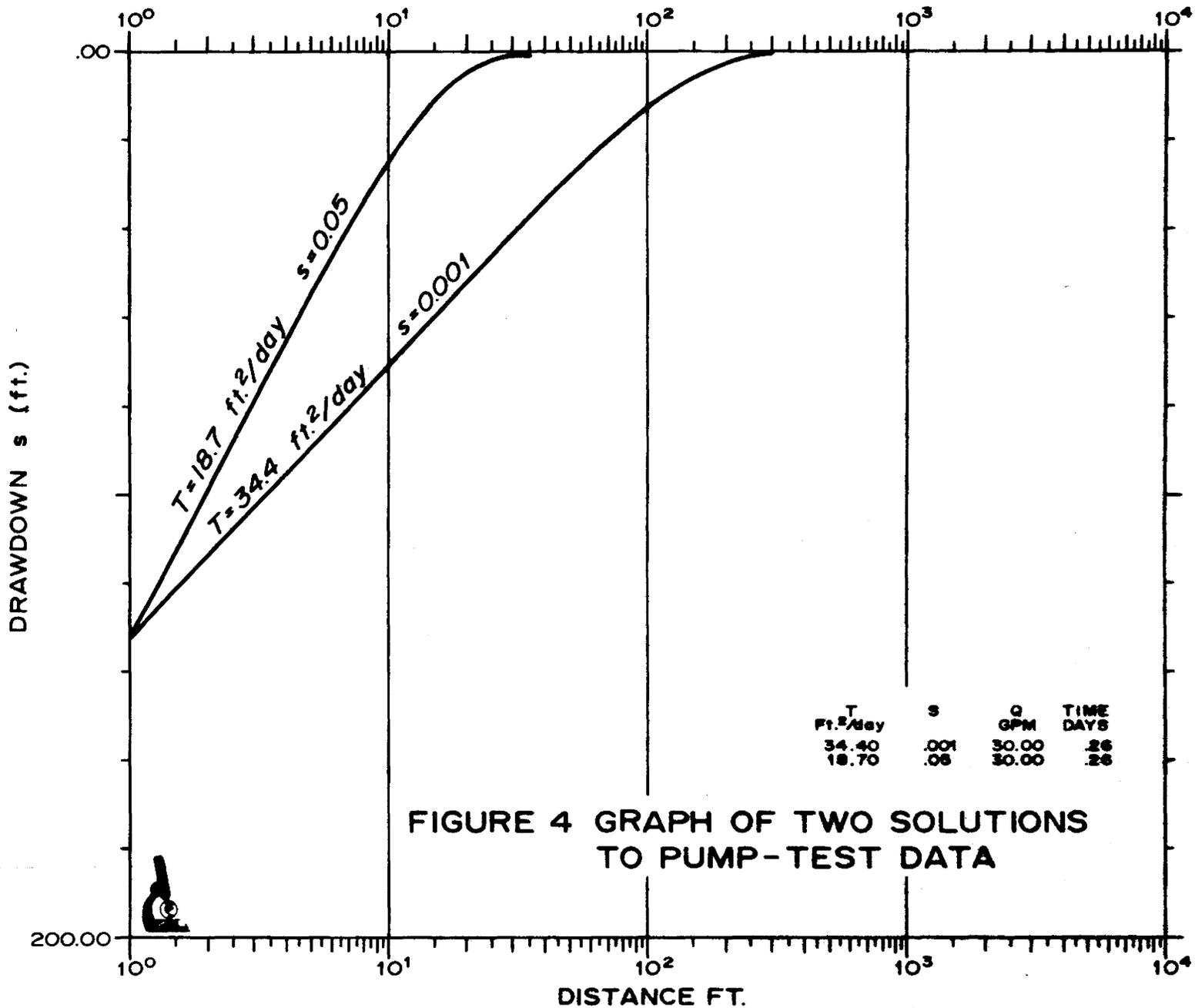


FIGURE 4 GRAPH OF TWO SOLUTIONS TO PUMP-TEST DATA

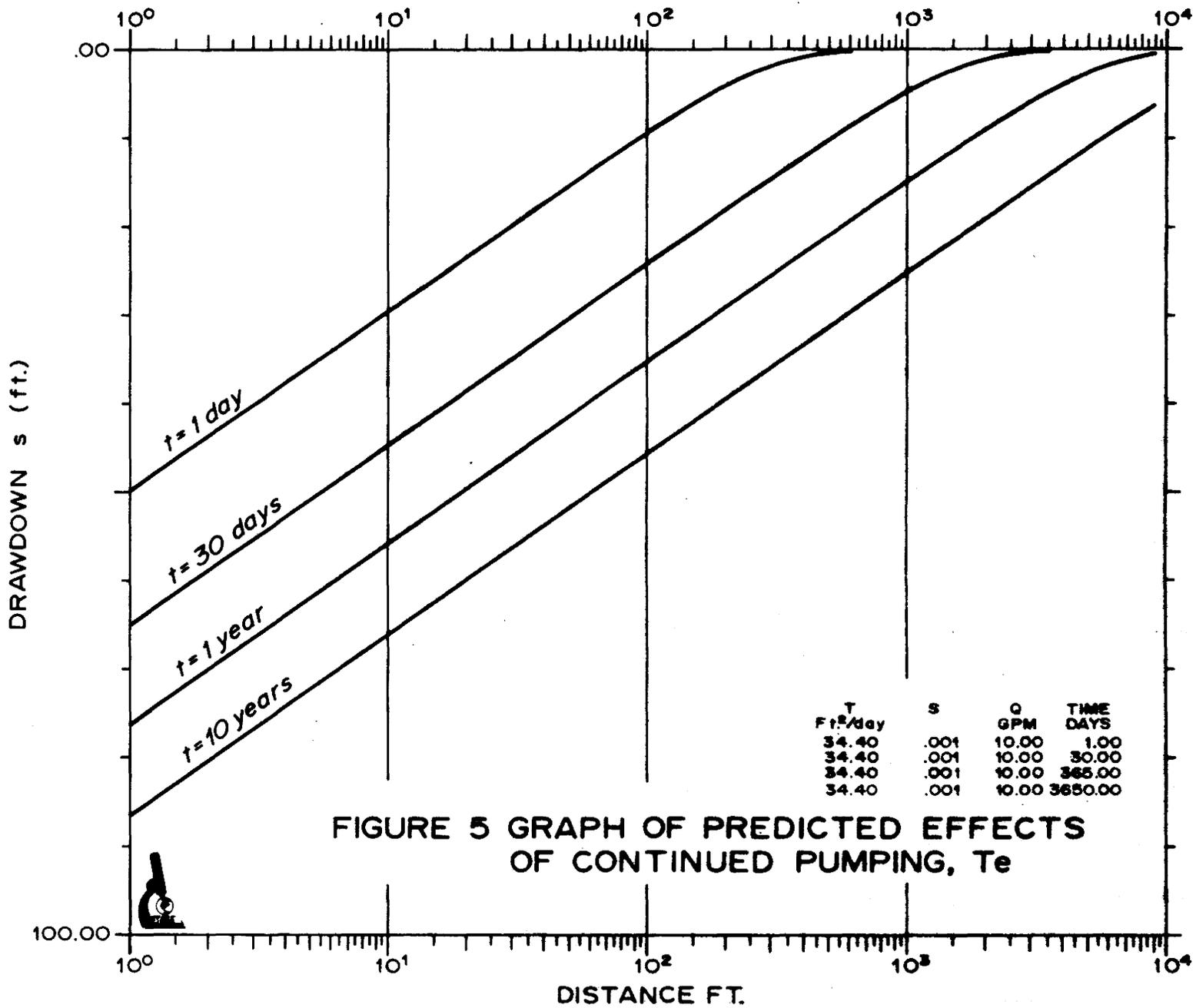


FIGURE 5 GRAPH OF PREDICTED EFFECTS OF CONTINUED PUMPING, T_e

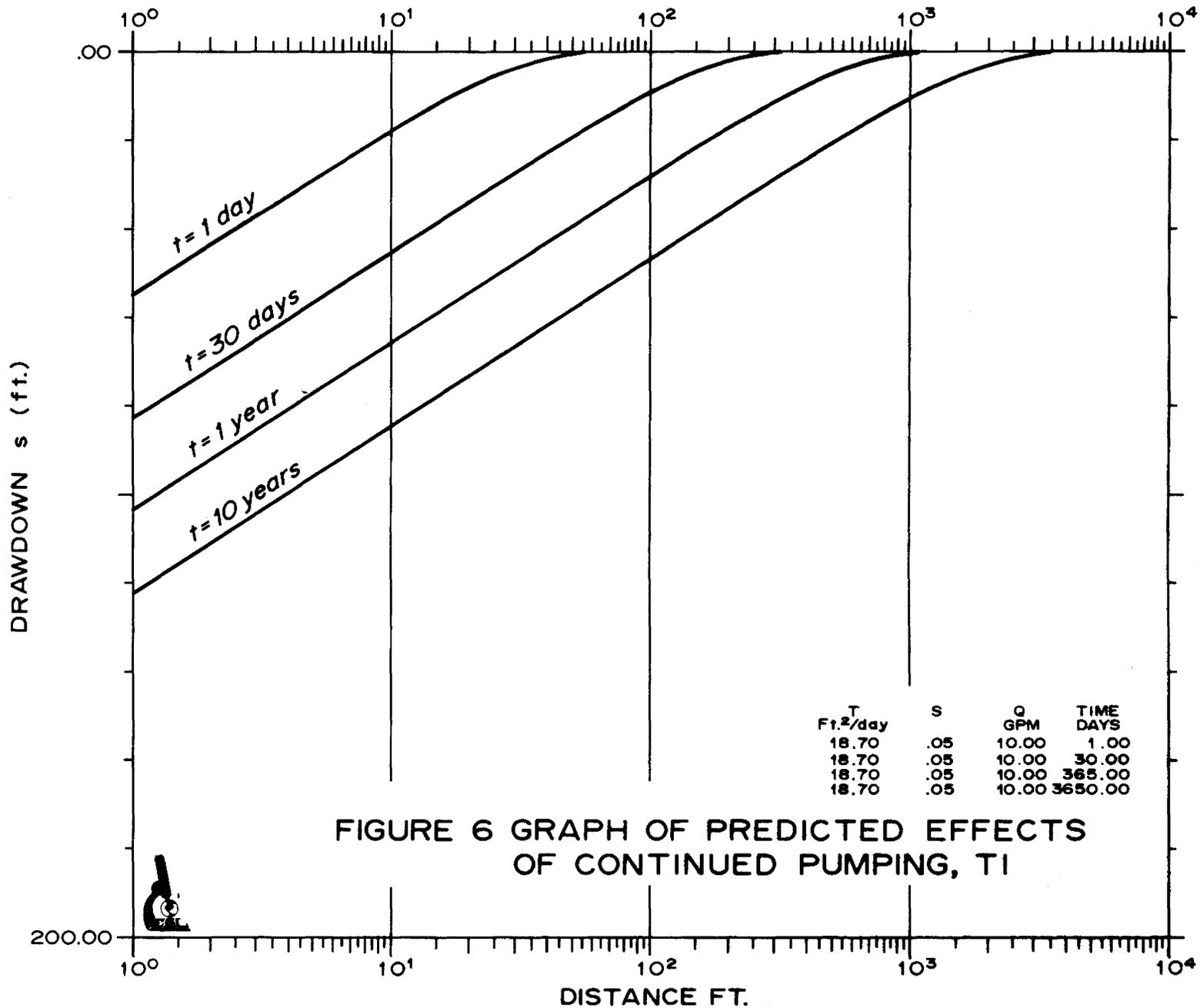


FIGURE 6 GRAPH OF PREDICTED EFFECTS OF CONTINUED PUMPING, T1

Table 1 Solution to pump-test data, Te

DRAWDOWN #	1		
T=	34.4000	S=	.0010 Q= 30.0000 TIME= .2600
#	DISTANCE	DRAWDOWN	
1	1,0000	132,361	
2	1,2000	127,490	
3	1,4000	123,372	
4	1,6000	119,804	
5	1,8000	116,657	
6	2,0000	113,843	
7	2,2000	111,296	
8	2,4000	108,972	
9	2,6000	106,834	
10	2,8000	104,854	
11	3,0000	103,011	
12	3,5000	98,894	
13	4,0000	95,327	
14	4,5000	92,182	
15	5,0000	89,369	
16	5,5000	86,824	
17	6,0000	84,501	
18	6,5000	82,365	
19	7,0000	80,387	
20	8,0000	76,825	
21	9,0000	73,685	
22	10,0000	70,877	
23	12,0000	66,022	
24	14,0000	61,922	
25	16,0000	58,377	
26	18,0000	55,255	
27	20,0000	52,468	
28	22,0000	49,953	
29	24,0000	47,662	
30	26,0000	45,561	
31	28,0000	43,621	
32	30,0000	41,820	
33	35,0000	37,821	
34	40,0000	34,391	
35	45,0000	31,398	
36	50,0000	28,755	
37	55,0000	26,397	
38	60,0000	24,277	
39	65,0000	22,360	
40	70,0000	20,617	
41	80,0000	17,567	
42	90,0000	14,995	
43	100,0000	12,806	
44	120,0000	9,327	
45	140,0000	6,755	
46	160,0000	4,849	
47	180,0000	3,442	
48	200,0000	2,413	
49	220,0000	1,669	
50	240,0000	1,138	
51	260,0000	.768	
52	280,0000	.521	
53	300,0000	.379	

Table 2 Solution to pump-test data, T1

DRAWDOWN #	2		
T=	18.7000	S=	.0500 Q= 30.0000 TIME= .2600
#	DISTANCE		DRAWDOWN
1	1,0000		132.432
2	1,2000		123.499
3	1,4000		115.955
4	1,6000		109.429
5	1,8000		103.683
6	2,0000		98.552
7	2,2000		93.921
8	2,4000		89.702
9	2,6000		85.830
10	2,8000		82.255
11	3,0000		78.937
12	3,5000		71.563
13	4,0000		65.232
14	4,5000		59.706
15	5,0000		54.819
16	5,5000		50.454
17	6,0000		46.526
18	6,5000		42.967
19	7,0000		39.727
20	8,0000		34.046
21	9,0000		29.237
22	10,0000		25.130
23	12,0000		18.555
24	14,0000		13.641
25	16,0000		9.954
26	18,0000		7.194
27	20,0000		5.142
28	22,0000		3.631
29	24,0000		2.531
30	26,0000		1.743
31	28,0000		1.193
32	30,0000		.835
33	35,0000		.825

UNABDOWN # 1				UNABDOWN # 2			
Te	30,000 Sz	.0010 Oz	10,000TIMEz	Te	30,000 Sz	.0010 Oz	10,000TIMEz
#	DISTANCE	DRAWDOWN	1.0000	#	DISTANCE	DRAWDOWN	30,0000
1	1,0000	50.119		1	1,0000	65.205	
2	1,2000	48.495		2	1,2000	63.641	
3	1,4000	47.122		3	1,4000	62.266	
4	1,6000	45.933		4	1,6000	61.079	
5	1,8000	44.884		5	1,8000	60.030	
6	2,0000	43.946		6	2,0000	59.091	
7	2,2000	43.097		7	2,2000	58.243	
8	2,4000	42.322		8	2,4000	57.468	
9	2,6000	41.609		9	2,6000	56.755	
10	2,8000	40.949		10	2,8000	56.095	
11	3,0000	40.335		11	3,0000	55.488	
12	3,5000	38.962		12	3,5000	54.187	
13	4,0000	37.773		13	4,0000	52.918	
14	4,5000	36.724		14	4,5000	51.669	
15	5,0000	35.786		15	5,0000	50.531	
16	5,5000	34.937		16	5,5000	50.082	
17	6,0000	34.162		17	6,0000	49.307	
18	6,5000	33.450		18	6,5000	48.594	
19	7,0000	32.798		19	7,0000	47.934	
20	8,0000	31.601		20	8,0000	46.745	
21	9,0000	30.553		21	9,0000	45.696	
22	10,0000	29.615		22	10,0000	44.758	
23	12,0000	27.993		23	12,0000	43.134	
24	14,0000	26.621		24	14,0000	41.761	
25	16,0000	25.434		25	16,0000	40.572	
26	18,0000	24.387		26	18,0000	39.523	
27	20,0000	23.451		27	20,0000	38.585	
28	22,0000	22.605		28	22,0000	37.736	
29	24,0000	21.833		29	24,0000	36.961	
30	26,0000	21.124		30	26,0000	36.248	
31	28,0000	20.467		31	28,0000	35.588	
32	30,0000	19.856		32	30,0000	34.974	
33	35,0000	18.494		33	35,0000	33.602	
34	40,0000	17.317		34	40,0000	32.413	
35	45,0000	16.281		35	45,0000	31.364	
36	50,0000	15.358		36	50,0000	30.426	
37	55,0000	14.526		37	55,0000	29.578	
38	60,0000	13.770		38	60,0000	28.804	
39	65,0000	13.077		39	65,0000	28.092	
40	70,0000	12.438		40	70,0000	27.432	
41	80,0000	11.297		41	80,0000	26.245	
42	90,0000	10.301		42	90,0000	25.197	
43	100,0000	9.422		43	100,0000	24.261	
44	120,0000	7.935		44	120,0000	22.642	
45	140,0000	6.720		45	140,0000	21.275	
46	160,0000	5.710		46	160,0000	20.092	
47	180,0000	4.860		47	180,0000	19.050	
48	200,0000	4.137		48	200,0000	18.120	
49	220,0000	3.521		49	220,0000	17.280	
50	240,0000	2.993		50	240,0000	16.515	
51	260,0000	2.540		51	260,0000	15.813	
52	280,0000	2.152		52	280,0000	15.165	
53	300,0000	1.818		53	300,0000	14.562	
54	350,0000	1.178		54	350,0000	13.224	
55	400,0000	.748		55	400,0000	12.075	
56	450,0000	.465		56	450,0000	11.071	
57	500,0000	.283		57	500,0000	10.182	
58	550,0000	.172		58	550,0000	9.388	
59	600,0000	.119		59	600,0000	8.673	
				60	650,0000	8.024	
				61	700,0000	7.433	
				62	800,0000	6.395	
				63	900,0000	5.514	
				64	1000,0000	4.768	
				65	1200,0000	3.547	
				66	1400,0000	2.634	
				67	1600,0000	1.943	
				68	1800,0000	1.422	
				69	2000,0000	1.029	
				70	2200,0000	.737	
				71	2400,0000	.521	
				72	2600,0000	.364	
				73	2800,0000	.253	
				74	3000,0000	.176	
				75	3500,0000	.124	

a - 1 day

b - 1 month

Table 3 Predicted drawdown, Te

DOWNDOWN #		J		10.0000TIMES 365.0000	
Ts	36.4000 Sz	.0010 Gz	DOWNDOWN	Ts	36.4000 Sz
N	DISTANCE			N	DISTANCE
1	1,0000	70.392		1	1,0000
2	1,2000	74.768		2	1,2000
3	1,4000	73.395		3	1,4000
4	1,6000	72.206		4	1,6000
5	1,8000	71.157		5	1,8000
6	2,0000	70.218		6	2,0000
7	2,2000	69.370		7	2,2000
8	2,4000	68.595		8	2,4000
9	2,6000	67.882		9	2,6000
10	2,8000	67.222		10	2,8000
11	3,0000	66.607		11	3,0000
12	3,5000	65.234		12	3,5000
13	4,0000	64.045		13	4,0000
14	4,5000	62.996		14	4,5000
15	5,0000	62.058		15	5,0000
16	5,5000	61.209		16	5,5000
17	6,0000	60.434		17	6,0000
18	6,5000	59.721		18	6,5000
19	7,0000	59.061		19	7,0000
20	8,0000	57.872		20	8,0000
21	9,0000	56.823		21	9,0000
22	10,0000	55.884		22	10,0000
23	12,0000	54.201		23	12,0000
24	14,0000	52.888		24	14,0000
25	16,0000	51.699		25	16,0000
26	18,0000	50.650		26	18,0000
27	20,0000	49.711		27	20,0000
28	22,0000	48.862		28	22,0000
29	24,0000	48.087		29	24,0000
30	26,0000	47.375		30	26,0000
31	28,0000	46.715		31	28,0000
32	30,0000	46.100		32	30,0000
33	35,0000	44.727		33	35,0000
34	40,0000	43.538		34	40,0000
35	45,0000	42.489		35	45,0000
36	50,0000	41.551		36	50,0000
37	55,0000	40.702		37	55,0000
38	60,0000	39.927		38	60,0000
39	65,0000	39.214		39	65,0000
40	70,0000	38.554		40	70,0000
41	80,0000	37.305		41	80,0000
42	90,0000	36.316		42	90,0000
43	100,0000	35.378		43	100,0000
44	120,0000	33.755		44	120,0000
45	140,0000	32.382		45	140,0000
46	160,0000	31.194		46	160,0000
47	180,0000	30.145		47	180,0000
48	200,0000	29.208		48	200,0000
49	220,0000	28.359		49	220,0000
50	240,0000	27.585		50	240,0000
51	260,0000	26.873		51	260,0000
52	280,0000	26.214		52	280,0000
53	300,0000	25.601		53	300,0000
54	350,0000	24.231		54	350,0000
55	400,0000	23.045		55	400,0000
56	450,0000	22.000		56	450,0000
57	500,0000	21.065		57	500,0000
58	550,0000	20.221		58	550,0000
59	600,0000	19.451		59	600,0000
60	650,0000	18.744		60	650,0000
61	700,0000	18.090		61	700,0000
62	800,0000	16.914		62	800,0000
63	900,0000	15.880		63	900,0000
64	1000,0000	14.958		64	1000,0000
65	1200,0000	13.373		65	1200,0000
66	1400,0000	12.045		66	1400,0000
67	1600,0000	10.908		67	1600,0000
68	1800,0000	9.918		68	1800,0000
69	2000,0000	9.045		69	2000,0000
70	2200,0000	8.287		70	2200,0000
71	2400,0000	7.569		71	2400,0000
72	2600,0000	6.949		72	2600,0000
73	2800,0000	6.369		73	2800,0000
74	3000,0000	5.849		74	3000,0000
75	3500,0000	4.736		75	3500,0000
76	4000,0000	3.837		76	4000,0000
77	4500,0000	3.104		77	4500,0000
78	5000,0000	2.505		78	5000,0000
79	5500,0000	2.014		79	5500,0000
80	6000,0000	1.612		80	6000,0000
81	6500,0000	1.295		81	6500,0000
82	7000,0000	1.018		82	7000,0000
83	8000,0000	.628		83	8000,0000
84	9000,0000	.378		84	9000,0000

DOWNDOWN #		J		10.0000TIMES 3650.0000	
Ts	36.4000 Sz	.0010 Gz	DOWNDOWN	Ts	36.4000 Sz
N	DISTANCE			N	DISTANCE
1	1,0000	80.645		1	1,0000
2	1,2000	85.821		2	1,2000
3	1,4000	83.649		3	1,4000
4	1,6000	82.459		4	1,6000
5	1,8000	81.410		5	1,8000
6	2,0000	80.472		6	2,0000
7	2,2000	79.623		7	2,2000
8	2,4000	78.848		8	2,4000
9	2,6000	78.135		9	2,6000
10	2,8000	77.475		10	2,8000
11	3,0000	76.861		11	3,0000
12	3,5000	75.488		12	3,5000
13	4,0000	74.299		13	4,0000
14	4,5000	73.250		14	4,5000
15	5,0000	72.311		15	5,0000
16	5,5000	71.462		16	5,5000
17	6,0000	70.688		17	6,0000
18	6,5000	69.975		18	6,5000
19	7,0000	69.315		19	7,0000
20	8,0000	68.125		20	8,0000
21	9,0000	67.076		21	9,0000
22	10,0000	66.138		22	10,0000
23	12,0000	64.514		23	12,0000
24	14,0000	63.141		24	14,0000
25	16,0000	61.952		25	16,0000
26	18,0000	60.903		26	18,0000
27	20,0000	59.965		27	20,0000
28	22,0000	59.116		28	22,0000
29	24,0000	58.341		29	24,0000
30	26,0000	57.628		30	26,0000
31	28,0000	56.968		31	28,0000
32	30,0000	56.354		32	30,0000
33	35,0000	54.981		33	35,0000
34	40,0000	53.792		34	40,0000
35	45,0000	52.743		35	45,0000
36	50,0000	51.804		36	50,0000
37	55,0000	50.955		37	55,0000
38	60,0000	50.180		38	60,0000
39	65,0000	49.468		39	65,0000
40	70,0000	48.808		40	70,0000
41	80,0000	47.618		41	80,0000
42	90,0000	46.569		42	90,0000
43	100,0000	45.631		43	100,0000
44	120,0000	44.007		44	120,0000
45	140,0000	42.634		45	140,0000
46	160,0000	41.445		46	160,0000
47	180,0000	40.396		47	180,0000
48	200,0000	39.458		48	200,0000
49	220,0000	38.609		49	220,0000
50	240,0000	37.834		50	240,0000
51	260,0000	37.122		51	260,0000
52	280,0000	36.462		52	280,0000
53	300,0000	35.847		53	300,0000
54	350,0000	34.475		54	350,0000
55	400,0000	33.286		55	400,0000
56	450,0000	32.237		56	450,0000
57	500,0000	31.299		57	500,0000
58	550,0000	30.451		58	550,0000
59	600,0000	29.676		59	600,0000
60	650,0000	28.964		60	650,0000
61	700,0000	28.305		61	700,0000
62	800,0000	27.117		62	800,0000
63	900,0000	26.069		63	900,0000
64	1000,0000	25.133		64	1000,0000
65	1200,0000	23.513		65	1200,0000
66	1400,0000	22.144		66	1400,0000
67	1600,0000	20.960		67	1600,0000
68	1800,0000	19.917		68	1800,0000
69	2000,0000	18.986		69	2000,0000
70	2200,0000	18.144		70	2200,0000
71	2400,0000	17.378		71	2400,0000
72	2600,0000	16.673		72	2600,0000
73	2800,0000	16.023		73	2800,0000
74	3000,0000	15.419		74	3000,0000
75	3500,0000	14.074		75	3500,0000
76	4000,0000	12.918		76	4000,0000
77	4500,0000	11.906		77	4500,0000
78	5000,0000	11.009		78	5000,0000
79	5500,0000	10.205		79	5500,0000
80	6000,0000	9.480		80	6000,0000
81	6500,0000	8.820		81	6500,0000
82	7000,0000	8.217		82	7000,0000
83	8000,0000	7.154		83	8000,0000
84	9000,0000	6.245		84	9000,0000

c - 1 year

d - 10 years

DRAWDOWN # 1			
Tz	10.7000 Sz	.0500 Sz	10.0000TIMES
#	DISTANCE	DRAWDOWN	1.0000
1	1,0000	55.103	
2	1,2000	52.179	
3	1,4000	49.656	
4	1,6000	47.472	
5	1,8000	45.540	
6	2,0000	43.824	
7	2,2000	42.267	
8	2,4000	40.846	
9	2,6000	39.540	
10	2,8000	38.332	
11	3,0000	37.208	
12	3,5000	34.700	
13	4,0000	32.533	
14	4,5000	30.626	
15	5,0000	28.926	
16	5,5000	27.393	
17	6,0000	25.998	
18	6,5000	24.721	
19	7,0000	23.543	
20	8,0000	21.436	
21	9,0000	19.597	
22	10,0000	17.972	
23	12,0000	15.216	
24	14,0000	12.960	
25	16,0000	11.077	
26	18,0000	9.486	
27	20,0000	8.129	
28	22,0000	6.966	
29	24,0000	5.965	
30	26,0000	5.101	
31	28,0000	4.355	
32	30,0000	3.710	
33	35,0000	2.459	
34	40,0000	1.601	
35	45,0000	1.022	
36	50,0000	.639	
37	55,0000	.394	
38	60,0000	.254	
39	65,0000	.214	

DRAWDOWN # 2			
Tz	10.7000 Sz	.0500 Sz	10.0000TIMES
#	DISTANCE	DRAWDOWN	30.0000
1	1,0000	83.020	
2	1,2000	80.033	
3	1,4000	77.507	
4	1,6000	75.320	
5	1,8000	73.390	
6	2,0000	71.664	
7	2,2000	70.103	
8	2,4000	68.677	
9	2,6000	67.366	
10	2,8000	66.152	
11	3,0000	65.022	
12	3,5000	62.497	
13	4,0000	60.310	
14	4,5000	58.301	
15	5,0000	56.456	
16	5,5000	54.695	
17	6,0000	53.071	
18	6,5000	51.561	
19	7,0000	50.148	
20	8,0000	48.903	
21	9,0000	47.806	
22	10,0000	46.813	
23	12,0000	42.334	
24	14,0000	39.818	
25	16,0000	37.642	
26	18,0000	35.724	
27	20,0000	34.012	
28	22,0000	32.466	
29	24,0000	31.057	
30	26,0000	29.764	
31	28,0000	28.569	
32	30,0000	27.460	
33	35,0000	24.993	
34	40,0000	22.872	
35	45,0000	21.019	
36	50,0000	19.377	
37	55,0000	17.908	
38	60,0000	16.584	
39	65,0000	15.382	
40	70,0000	14.285	
41	80,0000	12.354	
42	90,0000	10.711	
43	100,0000	9.299	
44	120,0000	7.015	
45	140,0000	5.280	
46	160,0000	3.953	
47	180,0000	2.938	
48	200,0000	2.164	
49	220,0000	1.578	
50	240,0000	1.139	
51	260,0000	.812	
52	280,0000	.574	
53	300,0000	.403	
54	350,0000	.213	

a - 1 day

b - 1 month

Table 4 Predicted drawdown, TI

DRAWDOWN # 3			10.0000TIME= 360.00
Ts	10.7000 Sz	.0000 Sz	DRAWDOWN
1	1,0000	103.406	
2	1,2000	100.801	
3	1,4000	97.976	
4	1,6000	95.788	
5	1,8000	93.858	
6	2,0000	92.132	
7	2,2000	90.571	
8	2,4000	89.145	
9	2,6000	87.834	
10	2,8000	86.629	
11	3,0000	85.489	
12	3,2000	84.404	
13	3,4000	83.374	
14	3,6000	82.397	
15	3,8000	81.471	
16	4,0000	80.594	
17	4,2000	79.764	
18	4,4000	78.979	
19	4,6000	78.238	
20	4,8000	77.541	
21	5,0000	76.887	
22	5,2000	76.275	
23	5,4000	75.703	
24	5,6000	75.170	
25	5,8000	74.675	
26	6,0000	74.217	
27	6,2000	73.795	
28	6,4000	73.408	
29	6,6000	73.054	
30	6,8000	72.732	
31	7,0000	72.440	
32	7,2000	72.178	
33	7,4000	71.944	
34	7,6000	71.737	
35	7,8000	71.556	
36	8,0000	71.400	
37	8,2000	71.268	
38	8,4000	71.159	
39	8,6000	71.072	
40	8,8000	71.005	
41	9,0000	70.957	
42	9,2000	70.927	
43	9,4000	70.913	
44	9,6000	70.914	
45	9,8000	70.929	
46	10,0000	70.957	
47	10,2000	70.997	
48	10,4000	71.048	
49	10,6000	71.109	
50	10,8000	71.180	
51	11,0000	71.260	
52	11,2000	71.348	
53	11,4000	71.444	
54	11,6000	71.547	
55	11,8000	71.656	
56	12,0000	71.770	
57	12,2000	71.889	
58	12,4000	72.013	
59	12,6000	72.141	
60	12,8000	72.273	
61	13,0000	72.409	
62	13,2000	72.549	
63	13,4000	72.692	
64	13,6000	72.838	
65	13,8000	72.986	
66	14,0000	73.136	
67	14,2000	73.288	
68	14,4000	73.441	
69	14,6000	73.595	
70	14,8000	73.750	
71	15,0000	73.906	
72	15,2000	74.063	
73	15,4000	74.221	
74	15,6000	74.380	
75	15,8000	74.540	
76	16,0000	74.700	
77	16,2000	74.861	
78	16,4000	75.023	
79	16,6000	75.185	
80	16,8000	75.348	
81	17,0000	75.512	
82	17,2000	75.676	
83	17,4000	75.840	
84	17,6000	76.004	
85	17,8000	76.168	
86	18,0000	76.332	
87	18,2000	76.496	
88	18,4000	76.660	
89	18,6000	76.824	
90	18,8000	76.988	
91	19,0000	77.152	
92	19,2000	77.316	
93	19,4000	77.480	
94	19,6000	77.644	
95	19,8000	77.808	
96	20,0000	77.972	
97	20,2000	78.136	
98	20,4000	78.300	
99	20,6000	78.464	
100	20,8000	78.628	
101	21,0000	78.792	
102	21,2000	78.956	
103	21,4000	79.120	
104	21,6000	79.284	
105	21,8000	79.448	
106	22,0000	79.612	
107	22,2000	79.776	
108	22,4000	79.940	
109	22,6000	80.104	
110	22,8000	80.268	
111	23,0000	80.432	
112	23,2000	80.596	
113	23,4000	80.760	
114	23,6000	80.924	
115	23,8000	81.088	
116	24,0000	81.252	
117	24,2000	81.416	
118	24,4000	81.580	
119	24,6000	81.744	
120	24,8000	81.908	
121	25,0000	82.072	
122	25,2000	82.236	
123	25,4000	82.400	
124	25,6000	82.564	
125	25,8000	82.728	
126	26,0000	82.892	
127	26,2000	83.056	
128	26,4000	83.220	
129	26,6000	83.384	
130	26,8000	83.548	
131	27,0000	83.712	
132	27,2000	83.876	
133	27,4000	84.040	
134	27,6000	84.204	
135	27,8000	84.368	
136	28,0000	84.532	
137	28,2000	84.696	
138	28,4000	84.860	
139	28,6000	85.024	
140	28,8000	85.188	
141	29,0000	85.352	
142	29,2000	85.516	
143	29,4000	85.680	
144	29,6000	85.844	
145	29,8000	86.008	
146	30,0000	86.172	
147	30,2000	86.336	
148	30,4000	86.500	
149	30,6000	86.664	
150	30,8000	86.828	
151	31,0000	86.992	
152	31,2000	87.156	
153	31,4000	87.320	
154	31,6000	87.484	
155	31,8000	87.648	
156	32,0000	87.812	
157	32,2000	87.976	
158	32,4000	88.140	
159	32,6000	88.304	
160	32,8000	88.468	
161	33,0000	88.632	
162	33,2000	88.796	
163	33,4000	88.960	
164	33,6000	89.124	
165	33,8000	89.288	
166	34,0000	89.452	
167	34,2000	89.616	
168	34,4000	89.780	
169	34,6000	89.944	
170	34,8000	90.108	
171	35,0000	90.272	
172	35,2000	90.436	
173	35,4000	90.600	
174	35,6000	90.764	
175	35,8000	90.928	
176	36,0000	91.092	
177	36,2000	91.256	
178	36,4000	91.420	
179	36,6000	91.584	
180	36,8000	91.748	
181	37,0000	91.912	
182	37,2000	92.076	
183	37,4000	92.240	
184	37,6000	92.404	
185	37,8000	92.568	
186	38,0000	92.732	
187	38,2000	92.896	
188	38,4000	93.060	
189	38,6000	93.224	
190	38,8000	93.388	
191	39,0000	93.552	
192	39,2000	93.716	
193	39,4000	93.880	
194	39,6000	94.044	
195	39,8000	94.208	
196	40,0000	94.372	
197	40,2000	94.536	
198	40,4000	94.700	
199	40,6000	94.864	
200	40,8000	95.028	
201	41,0000	95.192	
202	41,2000	95.356	
203	41,4000	95.520	
204	41,6000	95.684	
205	41,8000	95.848	
206	42,0000	96.012	
207	42,2000	96.176	
208	42,4000	96.340	
209	42,6000	96.504	
210	42,8000	96.668	
211	43,0000	96.832	
212	43,2000	96.996	
213	43,4000	97.160	
214	43,6000	97.324	
215	43,8000	97.488	
216	44,0000	97.652	
217	44,2000	97.816	
218	44,4000	97.980	
219	44,6000	98.144	
220	44,8000	98.308	
221	45,0000	98.472	
222	45,2000	98.636	
223	45,4000	98.800	
224	45,6000	98.964	
225	45,8000	99.128	
226	46,0000	99.292	
227	46,2000	99.456	
228	46,4000	99.620	
229	46,6000	99.784	
230	46,8000	99.948	
231	47,0000	100.112	
232	47,2000	100.276	
233	47,4000	100.440	
234	47,6000	100.604	
235	47,8000	100.768	
236	48,0000	100.932	
237	48,2000	101.096	
238	48,4000	101.260	
239	48,6000	101.424	
240	48,8000	101.588	
241	49,0000	101.752	
242	49,2000	101.916	
243	49,4000	102.080	
244	49,6000	102.244	
245	49,8000	102.408	
246	50,0000	102.572	
247	50,2000	102.736	
248	50,4000	102.900	
249	50,6000	103.064	
250	50,8000	103.228	
251	51,0000	103.392	
252	51,2000	103.556	
253	51,4000	103.720	
254	51,6000	103.884	
255	51,8000	104.048	
256	52,0000	104.212	
257	52,2000	104.376	
258	52,4000	104.540	
259	52,6000	104.704	
260	52,8000	104.868	
261	53,0000	105.032	
262	53,2000	105.196	
263	53,4000	105.360	
264	53,6000	105.524	
265	53,8000	105.688	
266	54,0000	105.852	
267	54,2000	106.016	
268	54,4000	106.180	
269	54,6000	106.344	
270	54,8000	106.508	
271	55,0000	106.672	
272	55,2000	106.836	
273	55,4000	107.000	
274	55,6000	107.164	
275	55,8000	107.328	
276	56,0000	107.492	
277	56,2000	107.656	
278	56,4000	107.820	
279	56,6000	107.984	
280	56,8000	108.148	
281	57,0000	108.312	
282	57,2000	108.476	
283	57,4000	108.640	
284	57,6000	108.804	
285	57,8000	108.968	
286	58,0000	109.132	
287	58,2000	109.296	
288	58,4000	109.460	
289	58,6000	109.624	
290	58,8000	109.788	
291	59,0000	109.952	
292	59,2000	110.116	
293	59,4000	110.280	
294	59,6000	110.444	
295	59,8000	110.608	
296	60,0000	110.772	
297	60,2000	110.936	
298	60,4000	111.100	
299	60,6000	111.264	
300	60,8000	111.428	
301	61,0000	111.592	
302	61,2000	111.756	
303	61,4000	111.920	
304	61,6000	112.084	
305	61,8000	112.248	
306	62,0000	112.412	
307	62,2000	112.576	